

Introduction



Andy Penev

Construction Management

CityCenterDC | Parcel 1

Washington, D.C.



CityCenterDC | Parcel 1 Washington, D.C.

Project Overview

Andy Penev
Construction Management

Size: 257,500 SF
Location: Washington, D.C.
Project Cost: \$48 million
Contract Type: (4) GMP
Delivery Method: Design-Bid-Build
Schedule: 4/11 – 1/14



Developer: Hines | Archstone
General Contractor: Clark/Smoot (JV)
Arch. of Record: Shalom Baranes Associates
Design Architect: Foster + Partners



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Analysis #2: Electrical Redesign
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Analysis #1: SIPS

- Create a new phasing and sequencing plan for typical floor and implement through a Short Interval Production Schedule.

Analysis #2: Construction Analysis of Electrical Redesign

- Propose an alternative electrical distribution system design and analyze its construction impacts.

Analysis #3: Alternative Footbridge Installation

- Provide an alternative footbridge installation method to reduce cost and constructability issues.



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Analysis #1

Short Interval Production Schedule (SIPS)



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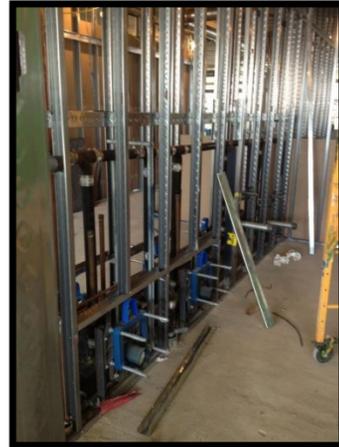
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Framing & Plumbing Rough In



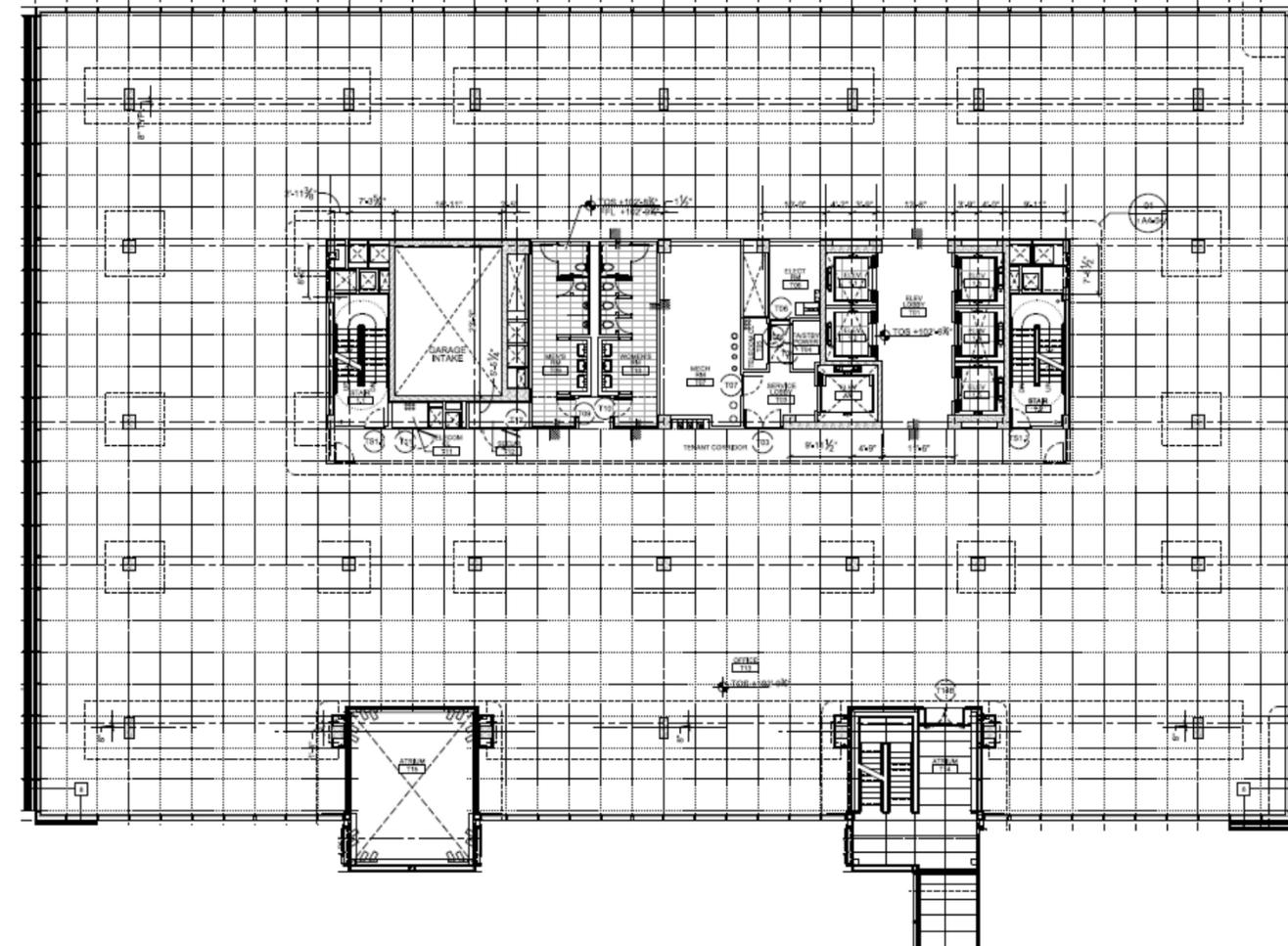
Risers



Mechanical Duct



AHU





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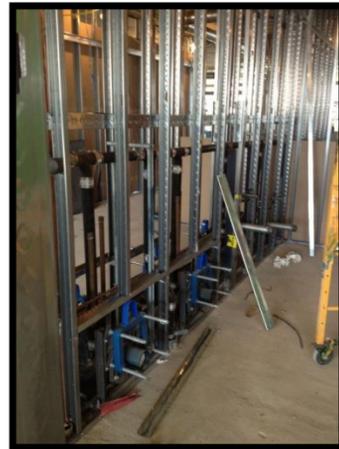
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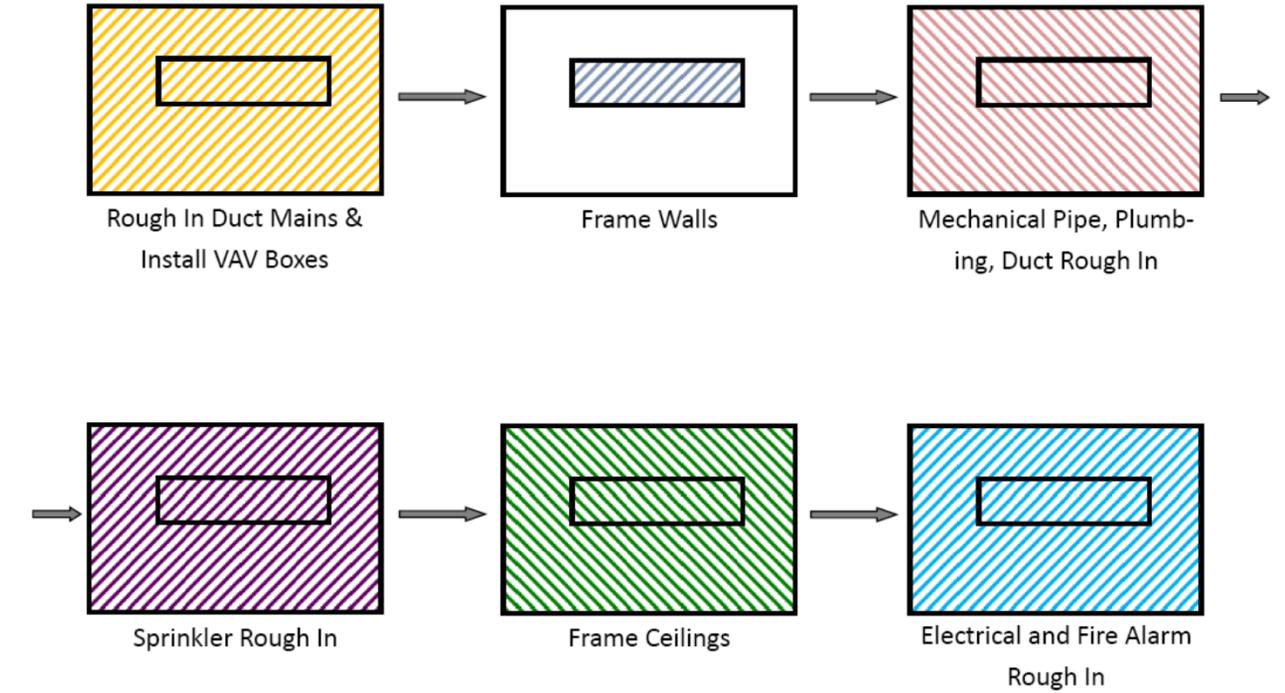
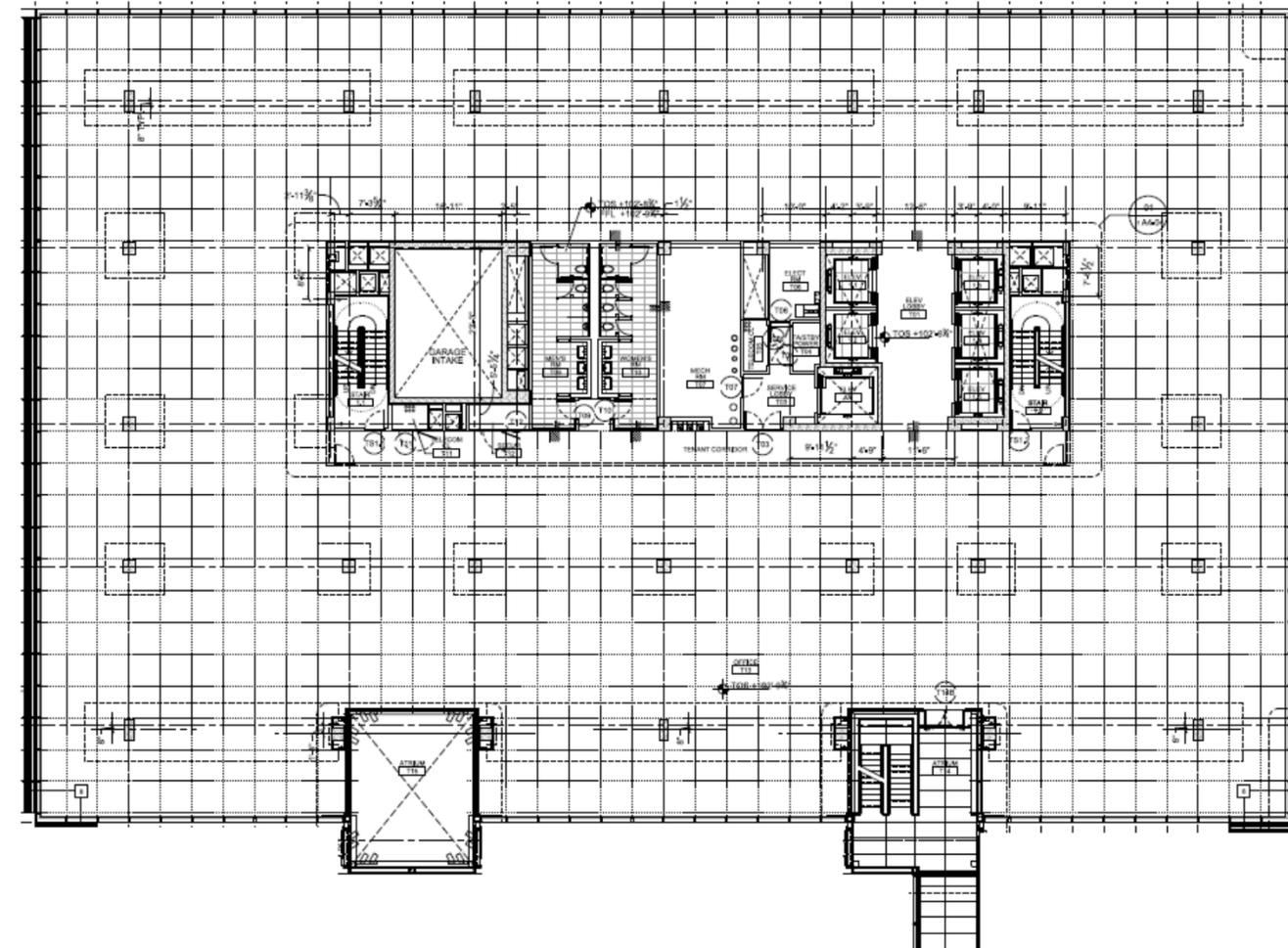
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New Phasing

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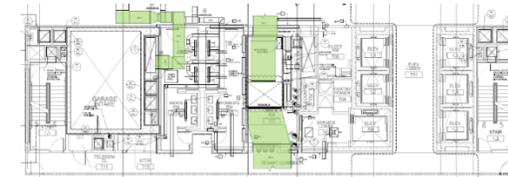
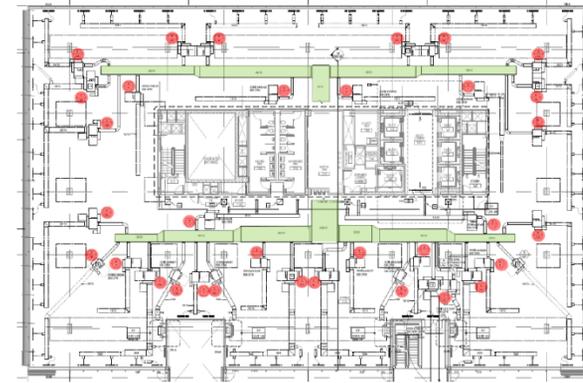
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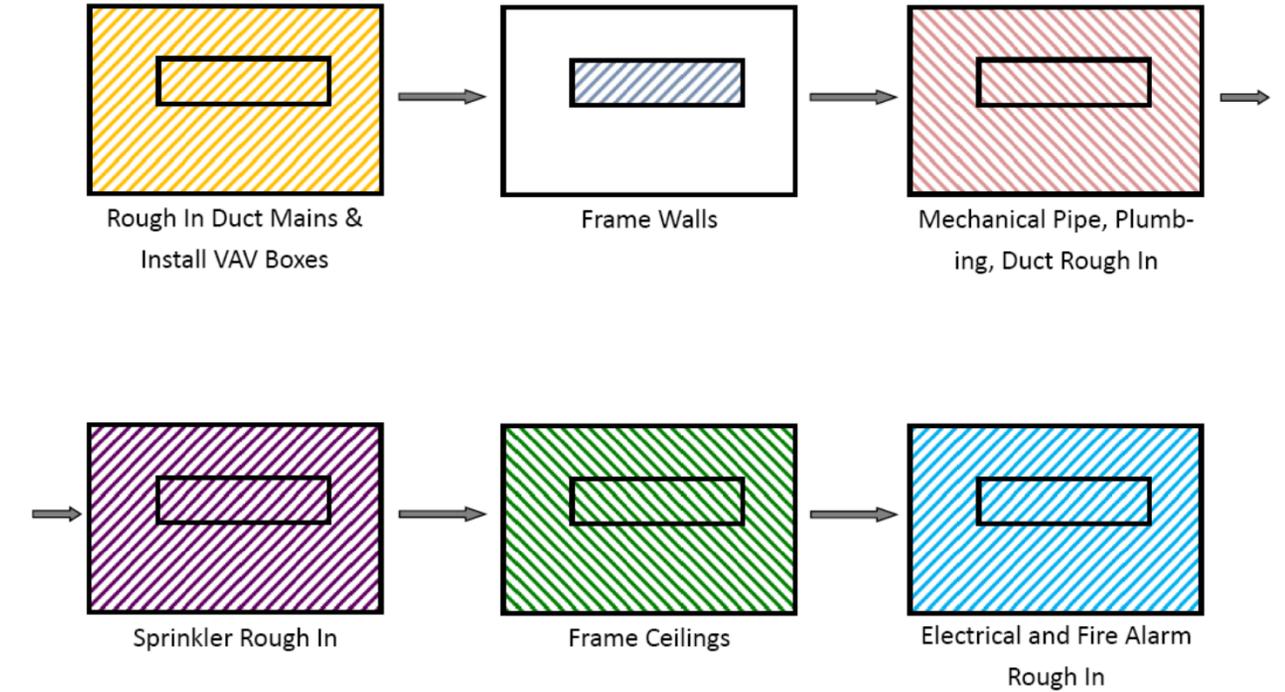
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- Identify Duct Mains
- Identify VAV Boxes





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New Phasing

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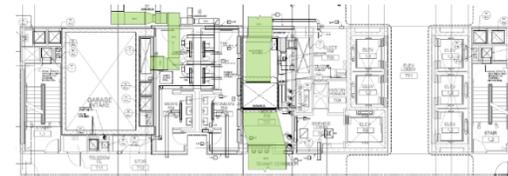
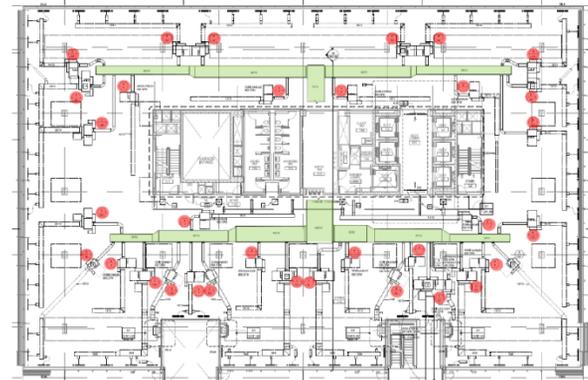
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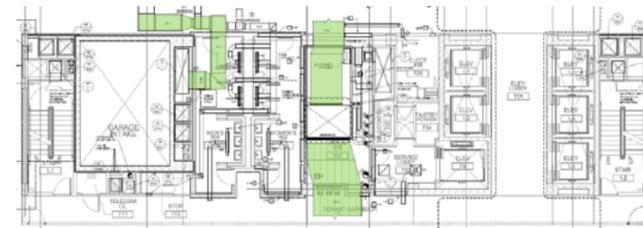
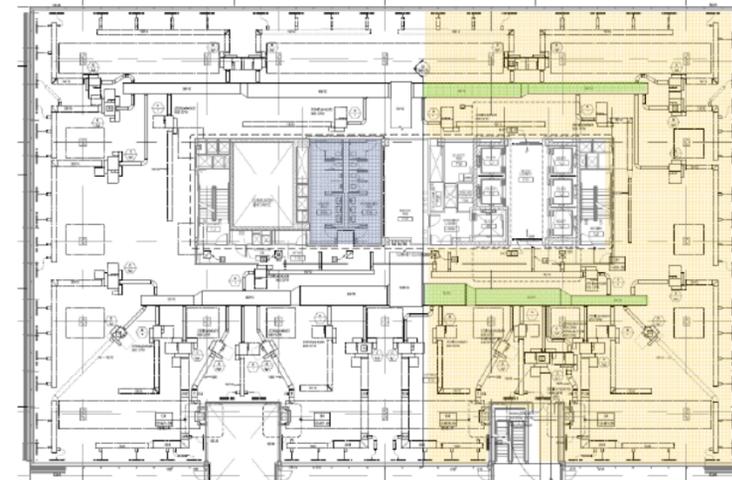
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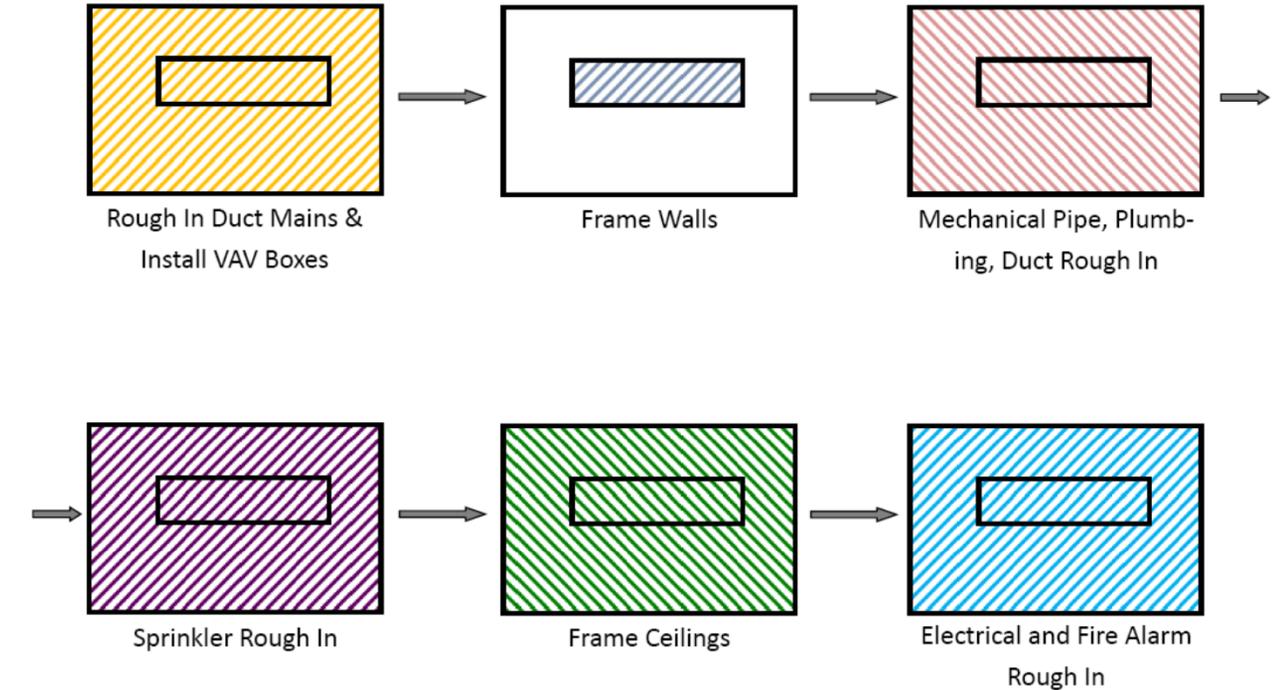
Install VAV Boxes



Lavatory Steel



Rough In Duct Mains





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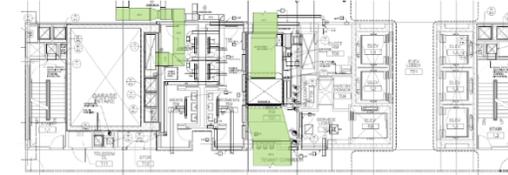
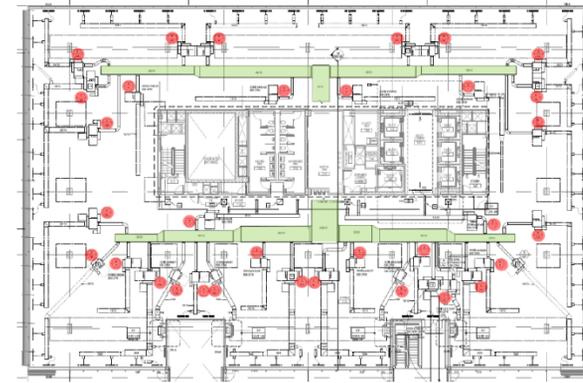
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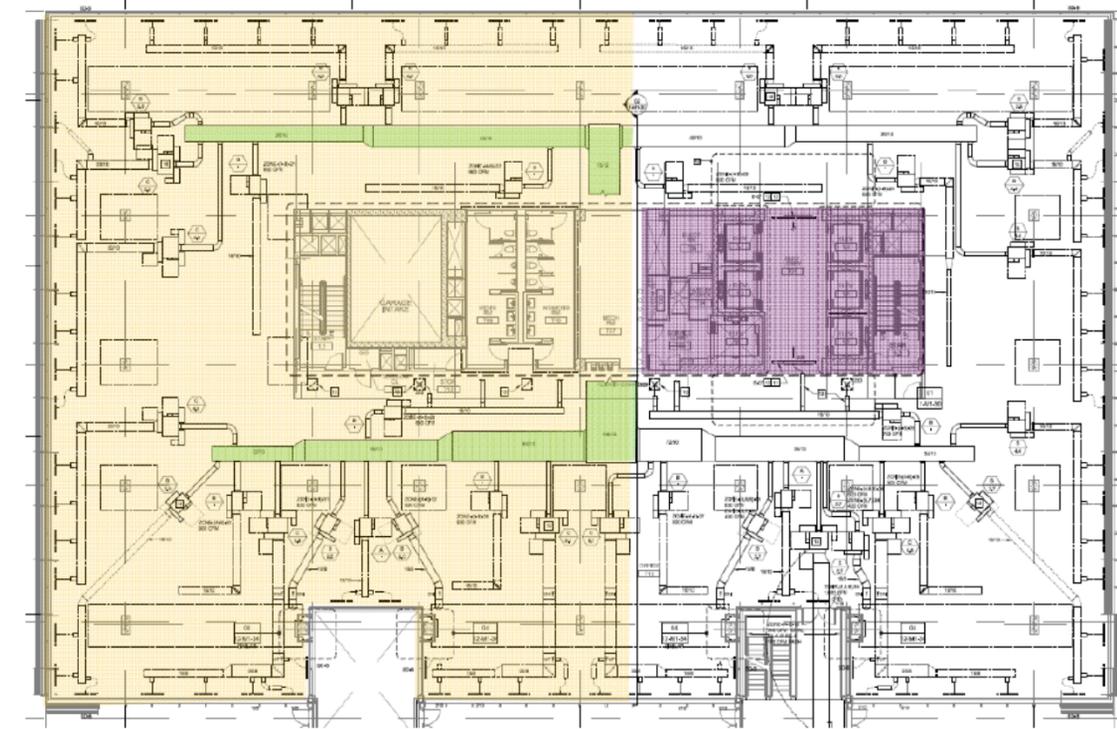
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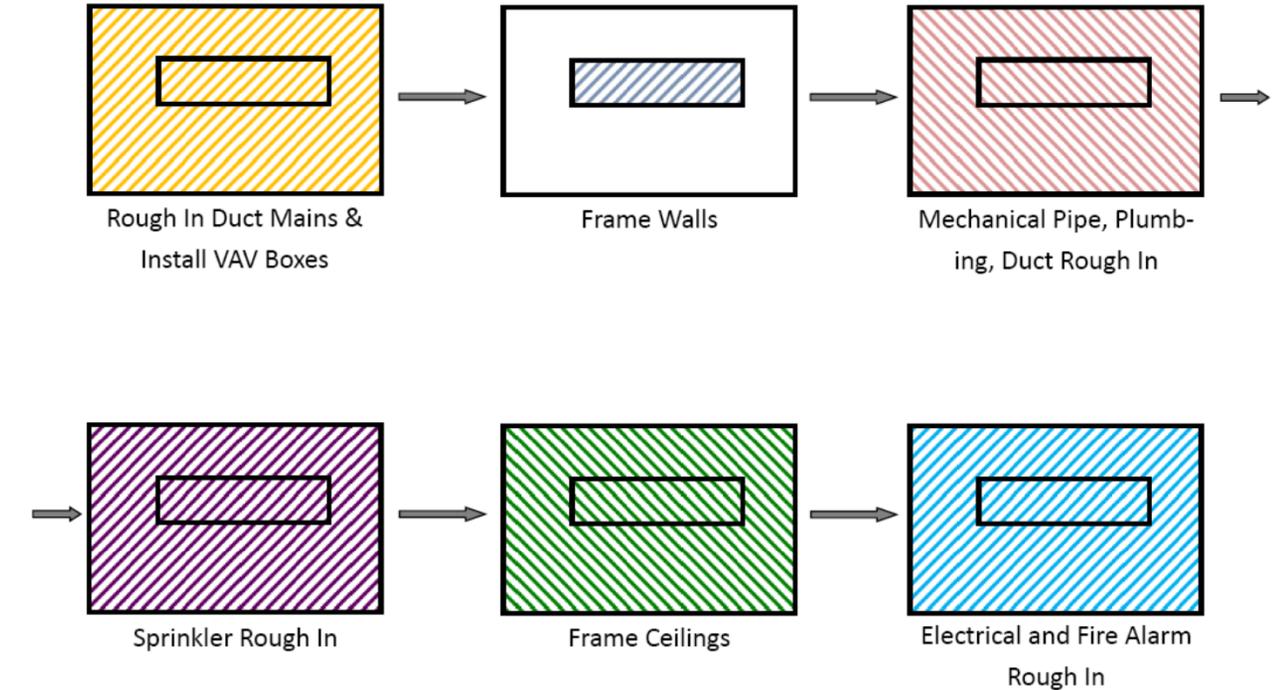
Install VAV Boxes



Frame Walls



Rough In Duct Mains





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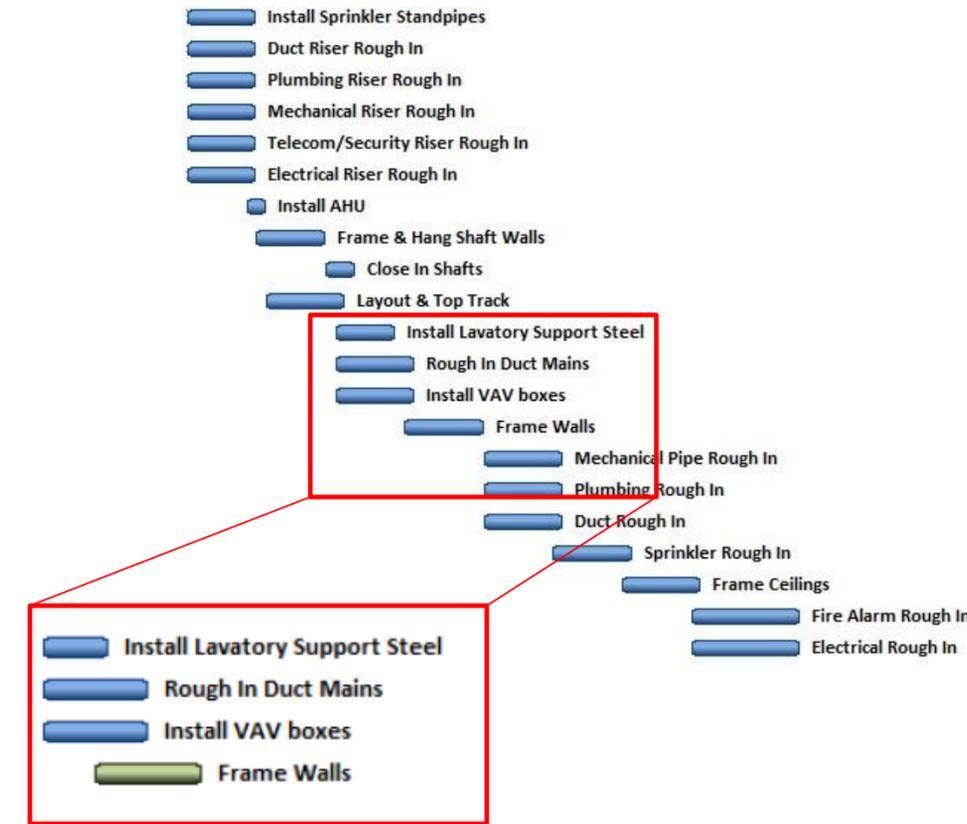
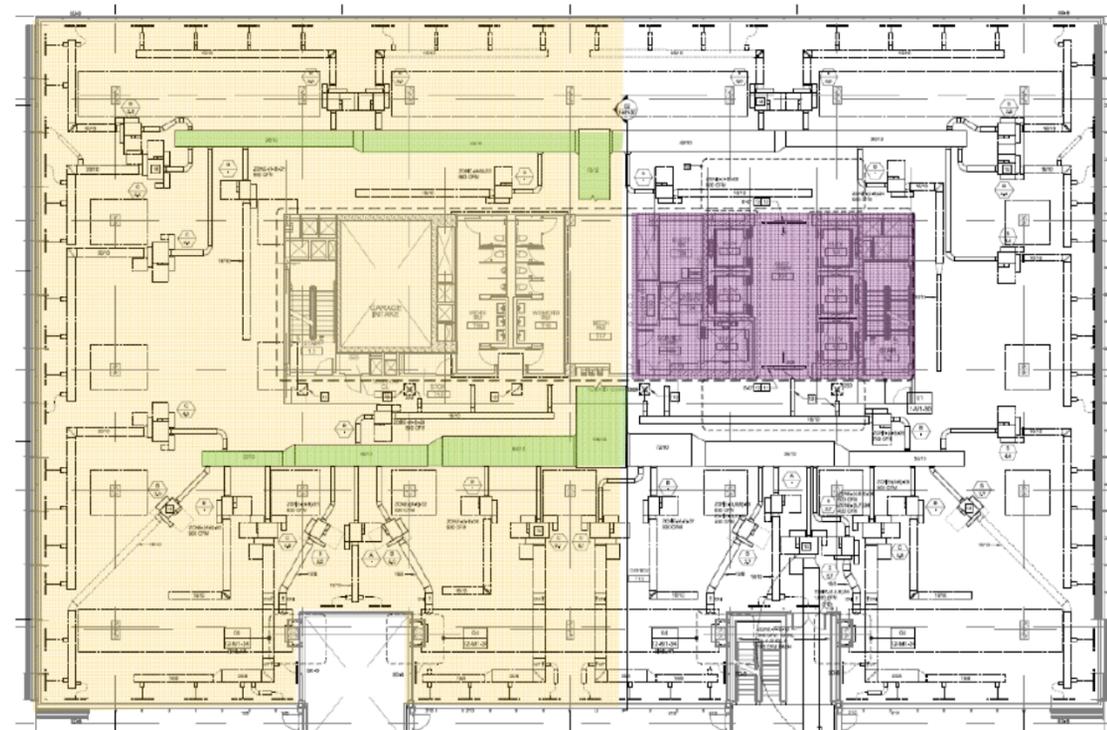
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- Create zones on each floor
- Crew stays in zone for given amount of time
- Creates efficient use of space
- Entire floor space is used

Important:

- Clean up
- Timely completion
- Material management





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Analysis #2

Construction Analysis of Electrical Redesign



Analysis #2: Electrical Redesign

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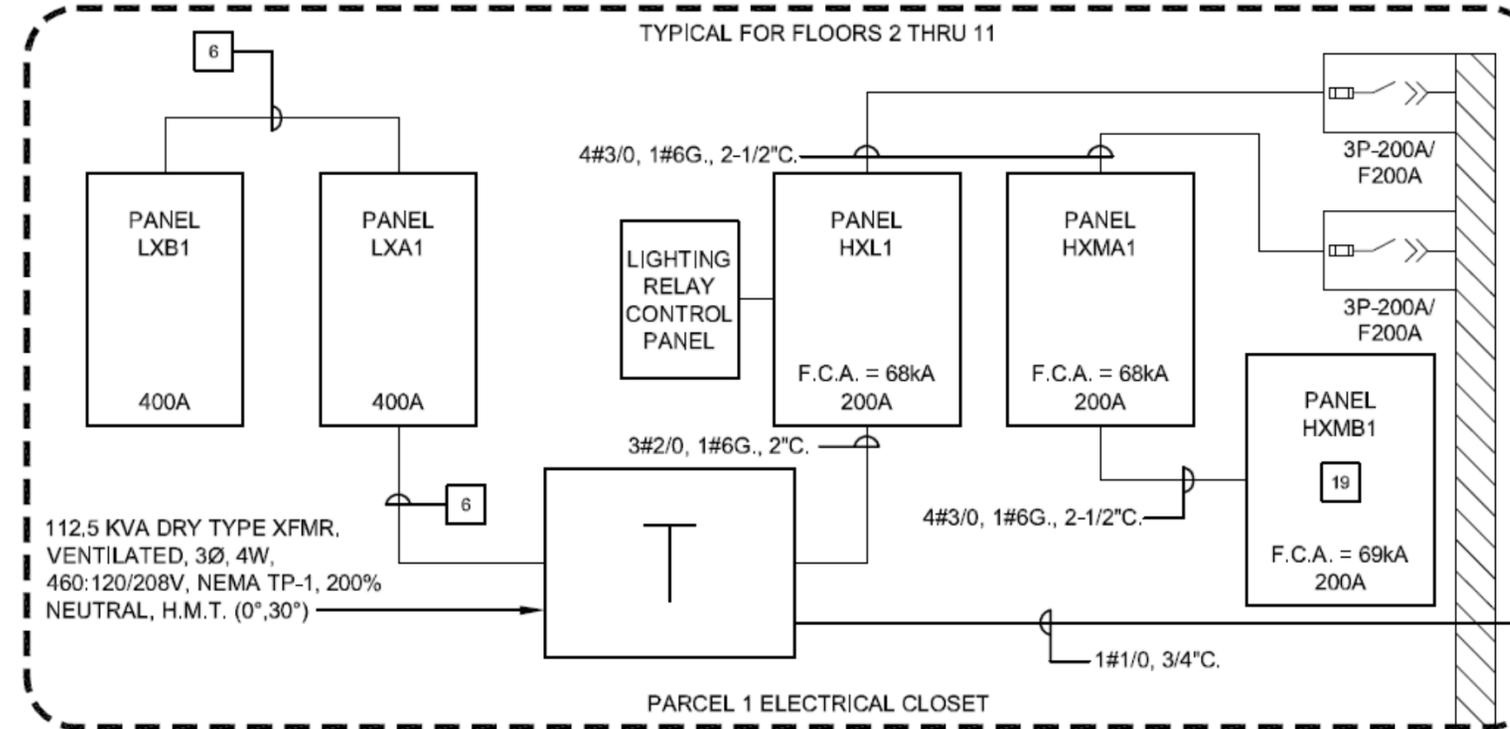
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- 2 Switchboards (4000A & 3000A)
- Total kVA = 5,248
 - 20.4 W/SF
- Separate retail feed
- Lighting + Receptacle load = 2,092 kVA
 - 7.7 W/SF
- 4000A SWBD busway to electrical closets
 - Took most of lighting and receptacle loads (1,902 kVA)



SWITCHBOARD MS12A LOADS:	
RECEPTACLES & FUTURE RECEPTACLES	1,570 KVA
LIGHTING & FUTURE LIGHTING	332 KVA
ELEVATORS	0 KVA
MISCELLANEOUS	11 KVA
* AIR CONDITIONING	0 KVA
FPTD MOTORS	345 KVA
DOMESTIC WATER HEATING	24 KVA
* ELECTRIC HEAT	891 KVA
TOTAL	3,173 KVA
* NONCOINCIDENT LOADS	(3,982A @ 460V, 3Ø)

SWITCHBOARD MS12C LOADS:	
RECEPTACLES & FUTURE RECEPTACLES	70 KVA
LIGHTING & FUTURE LIGHTING	120 KVA
ELEVATORS	397 KVA
MISCELLANEOUS	178 KVA
* AIR CONDITIONING	660 KVA
FPTD MOTORS	25 KVA
WATER CHILLING UNITS	465 KVA
DOMESTIC WATER HEATING	14 KVA
* ELECTRIC HEAT	0 KVA
FIRE PUMP	146 KVA
TOTAL	2,075 KVA
* NONCOINCIDENT LOADS	(2,604A @ 460V, 3Ø)



Analysis #2: Electrical Redesign

Redesign

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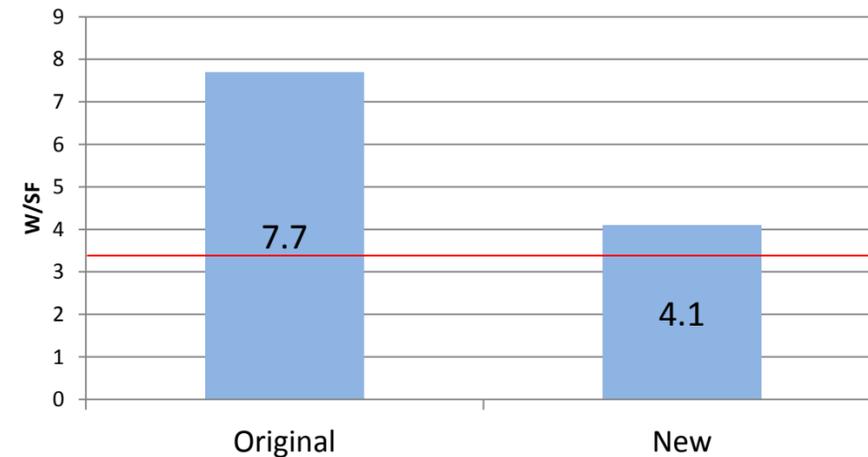
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Ltg. + Receptacle Power Density



- ASHRAE Maximum Lighting Power Density = 0.9 W/SF
- Receptacle Load = 2.4 W/SF

Total= 3.3 W/SF

	kVA Load	FLA	Voltage	Phase	SWBD Size
Initial SWBD	3173	3982	480	3	4000A
Revised SWBD	2373	2978	480	3	3000A

SWITCHBOARD MS12A LOADS:	
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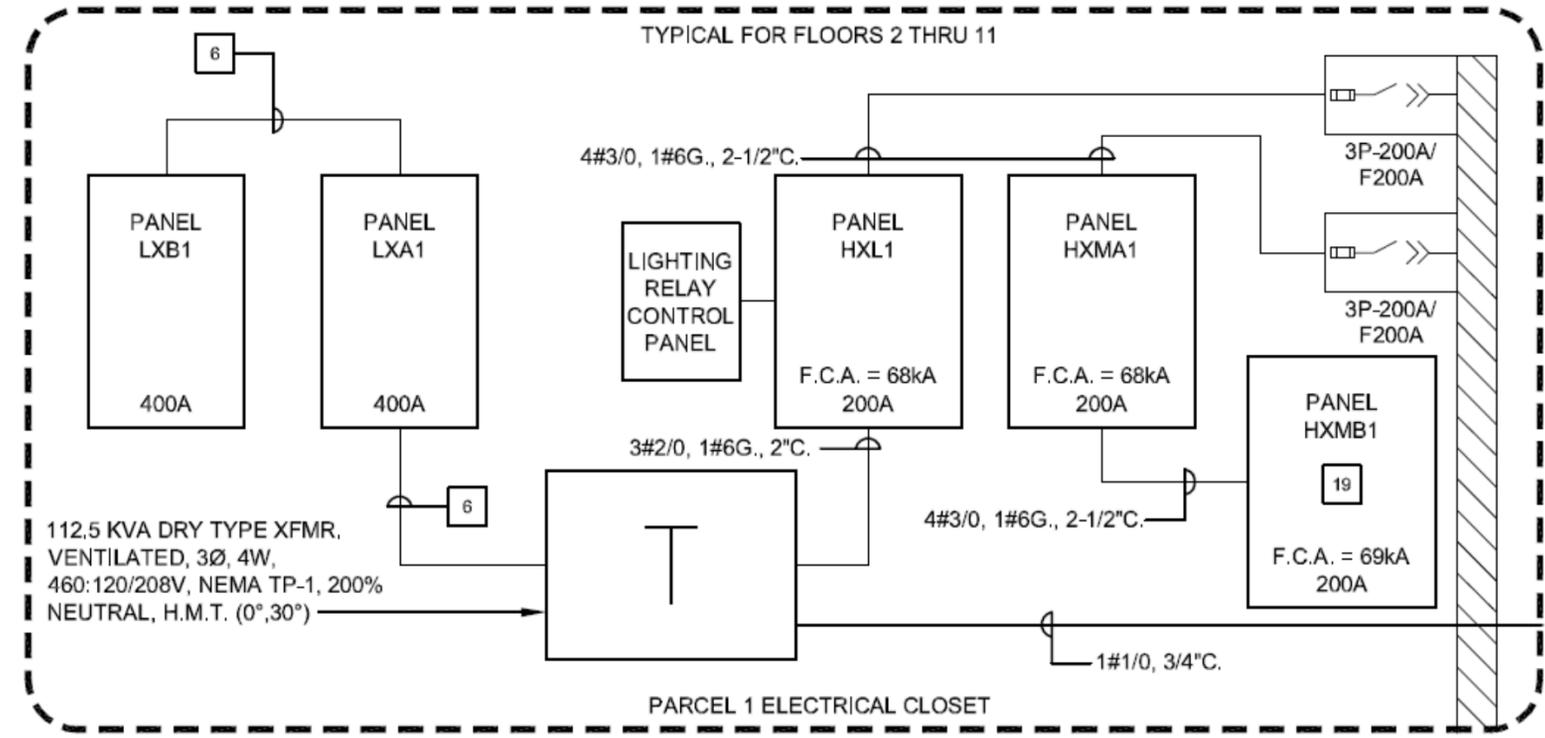
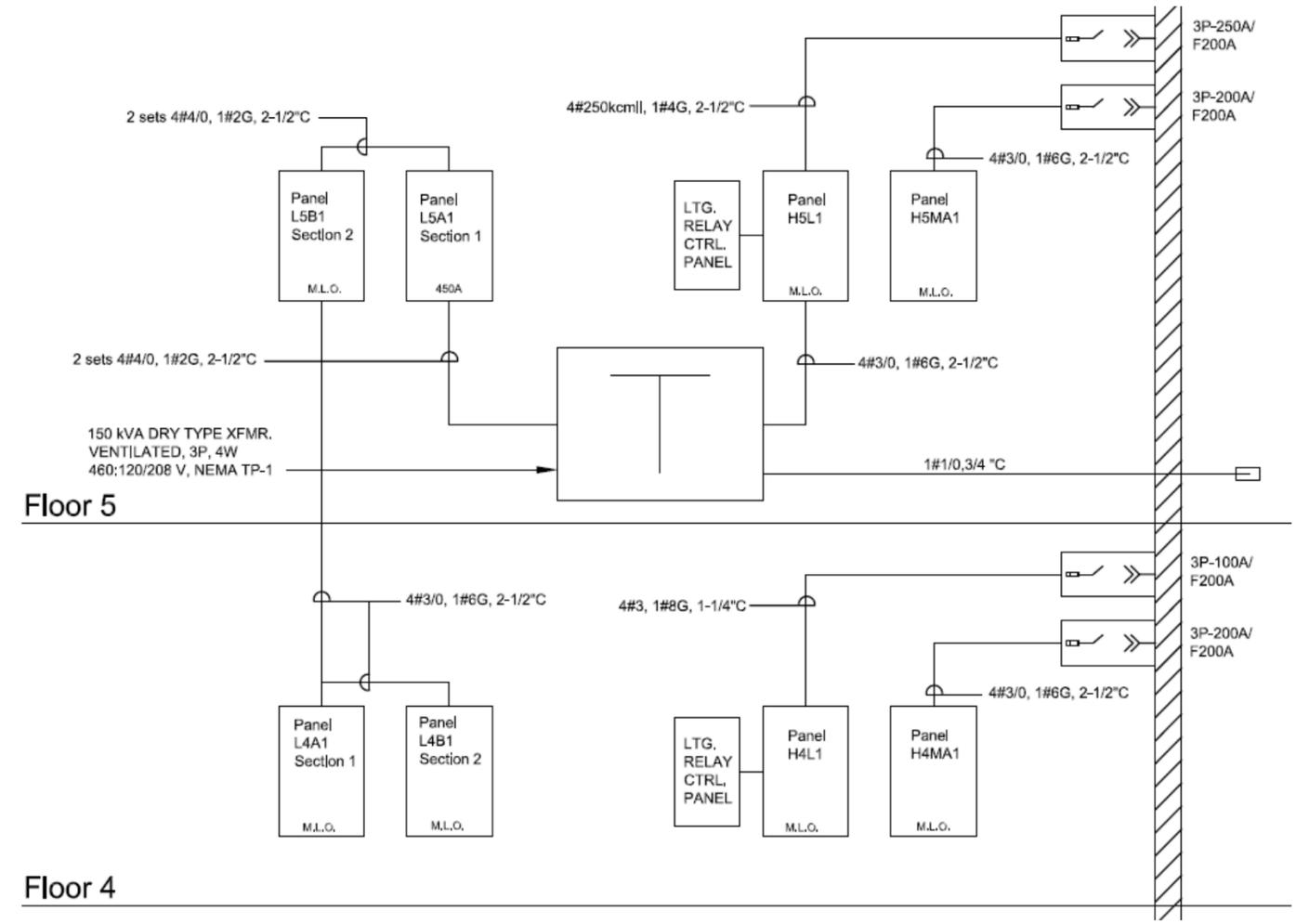
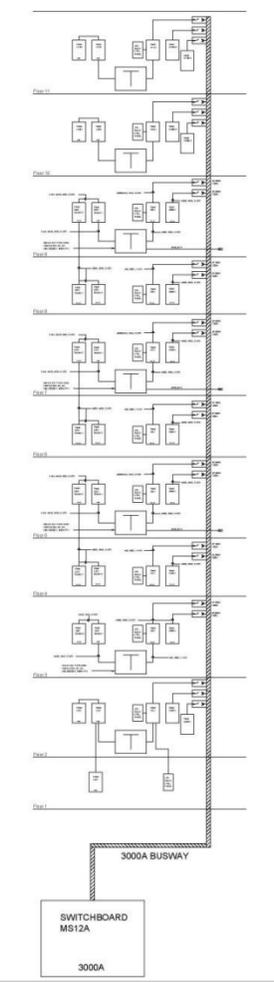
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- Eliminate XFMR on floors 4,6, & 8
 - Feed low voltage panels from floor above
- Floors 5,7, & 9 XFMR step up to 150kVa
- Feeders, plugs, breakers
- Coordination of cores
 - Fireproofing



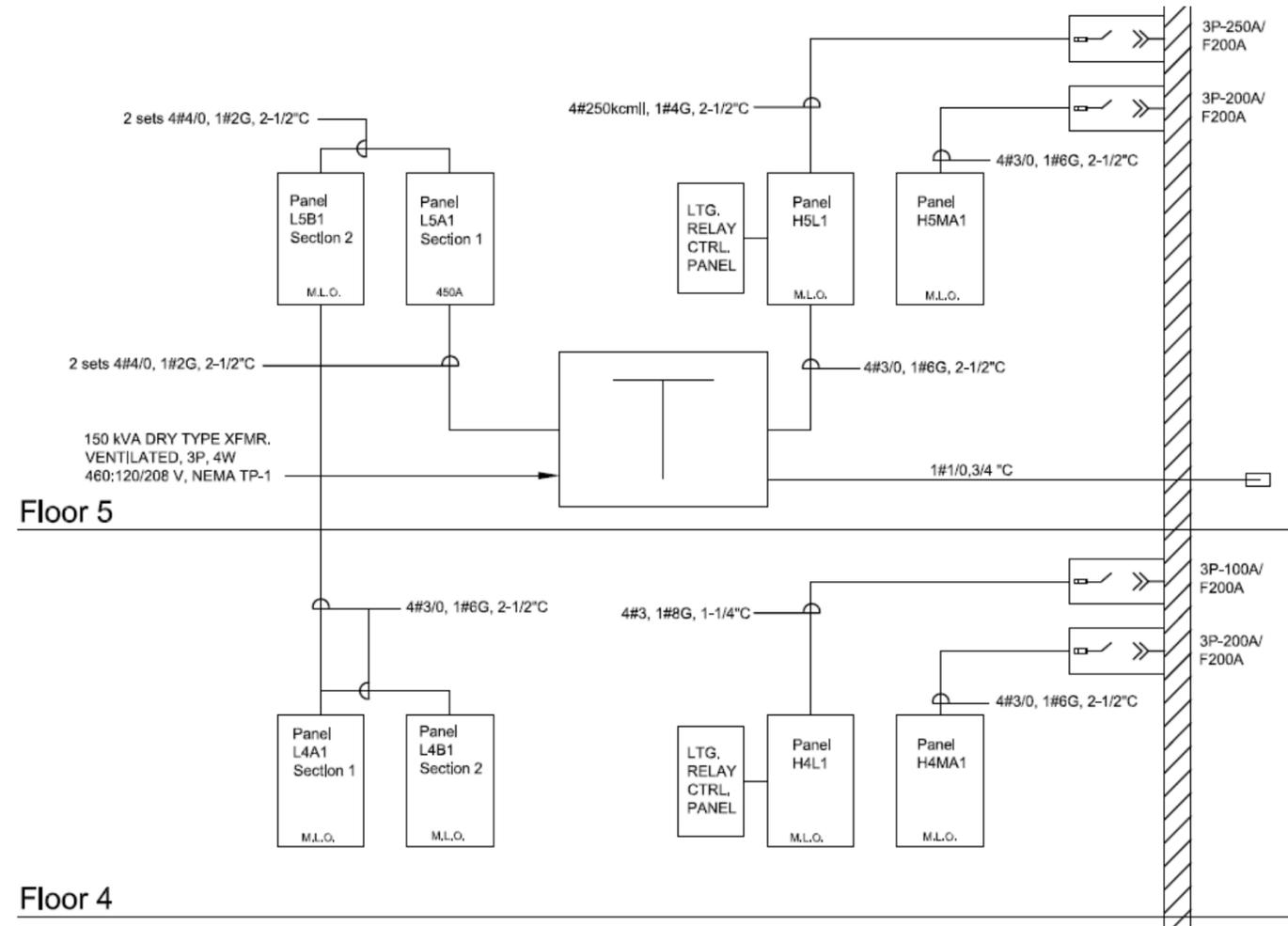
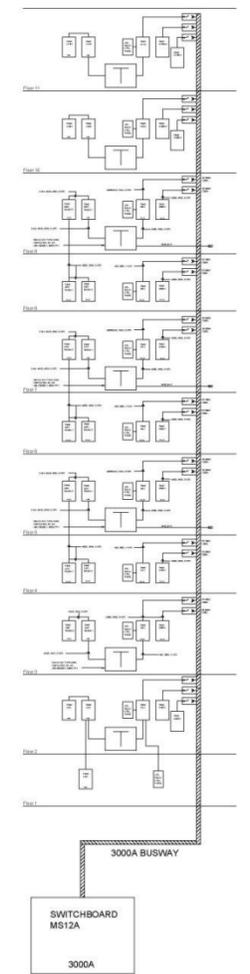


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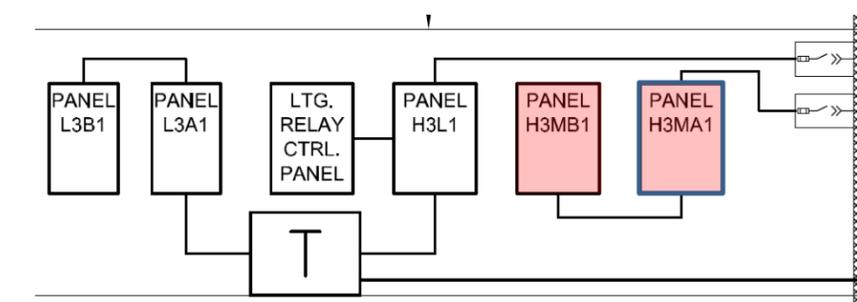
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 - Feed low voltage panels from floor above
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- Consolidation of HVAC panels



- Smaller XFMR from reduced loads on 3rd floor
 - Feeders

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Schedule

ELECTRICAL RISER ROUGH IN	Hours per Floor	Crew Size
Original Design (5 day duration)	76	2
Redesign Floor w/ XFMR	79.75	2
Redesign Floor w/o XFMR	31.42	1*

ELECTRICAL ROUGH IN	Hours per Floor	Crew Size
Original Design	149	4
Redesign Floor w/ XFMR	142.33	4
Redesign Floor w/o XFMR	148.33	4

Total labor hours saved: **182**

- Dependency
- Resource allocation

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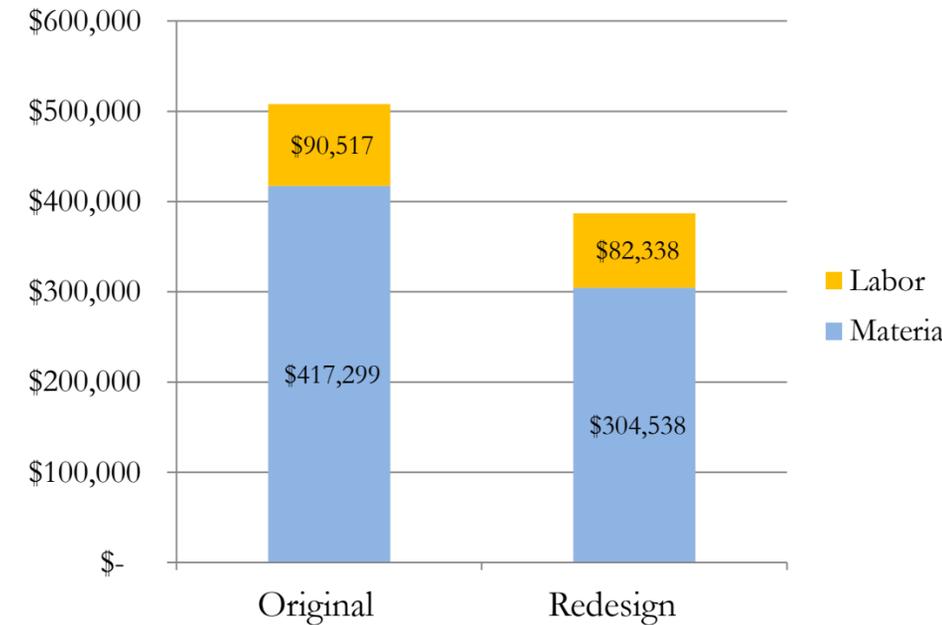
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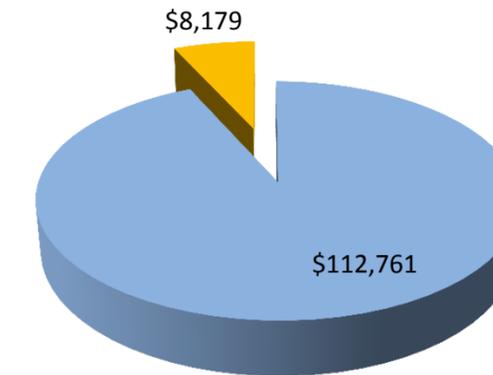
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Cost

Cost Comparison



Savings = **\$120,940**





Analysis #2: Electrical Redesign

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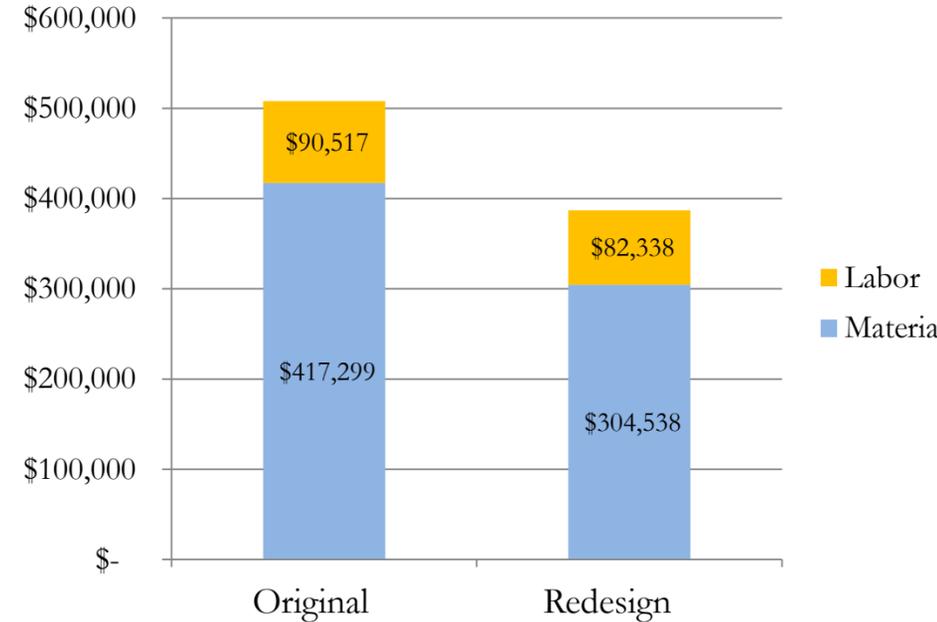
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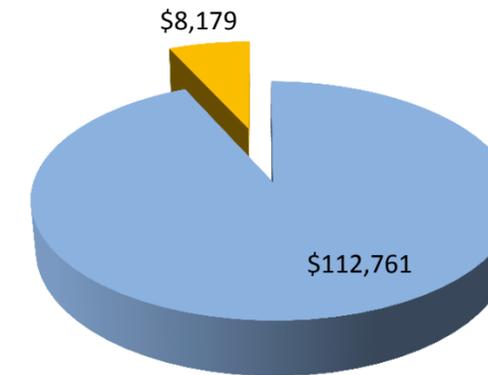
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Cost

Cost Comparison



Savings = **\$120,940**



Constructability

Item	Labor Hours
4000A Busway (59.4 lb/ft)	719.9
3000A Busway (42.7 lb/ft)	626
Labor Savings	93.9

- Horizontal bus runs quicker with lighter material
 - Less panels
 - Less XFMRs
- Less cluttered electrical closet
 - Coring coordination
 - Fireproofing

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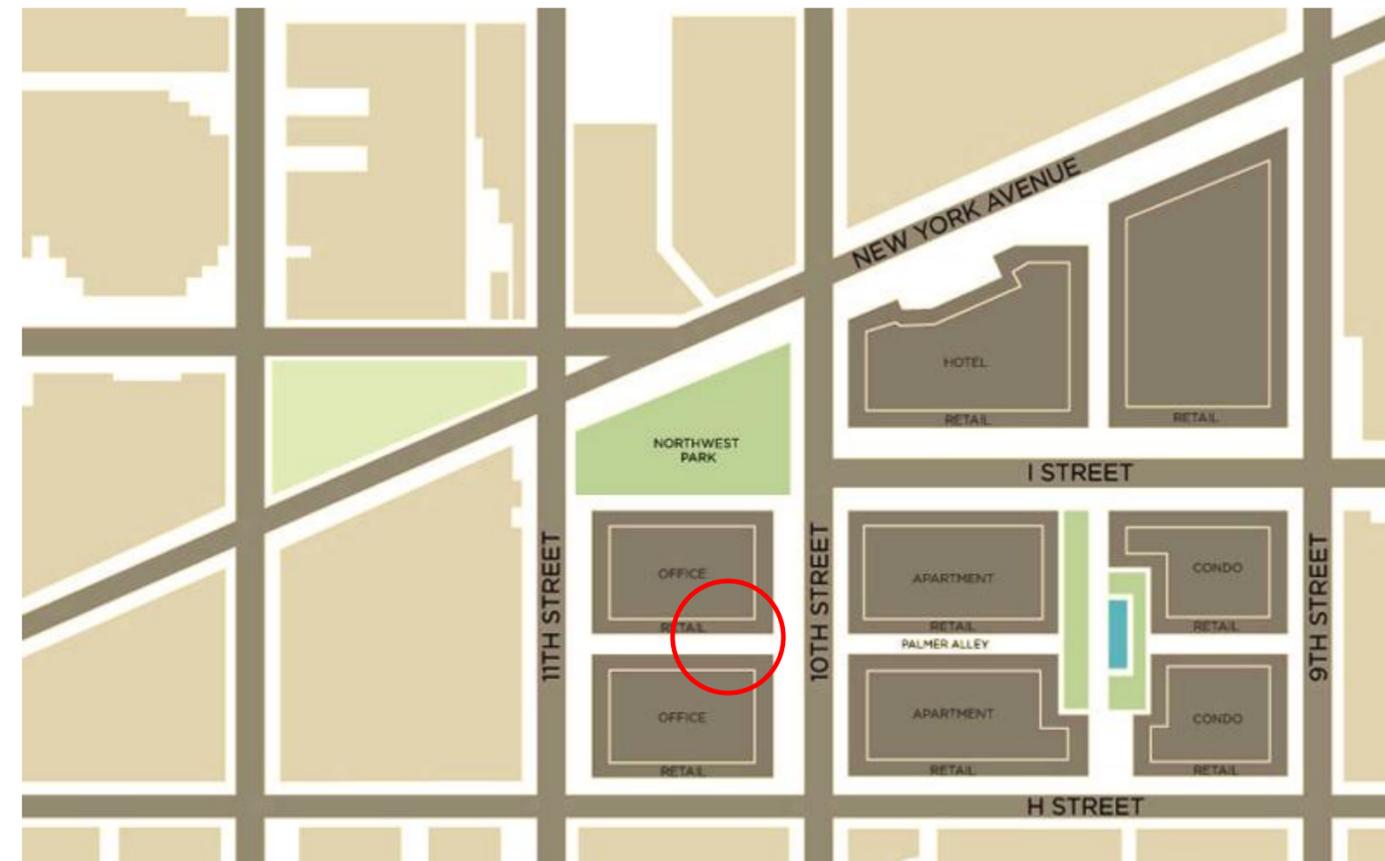
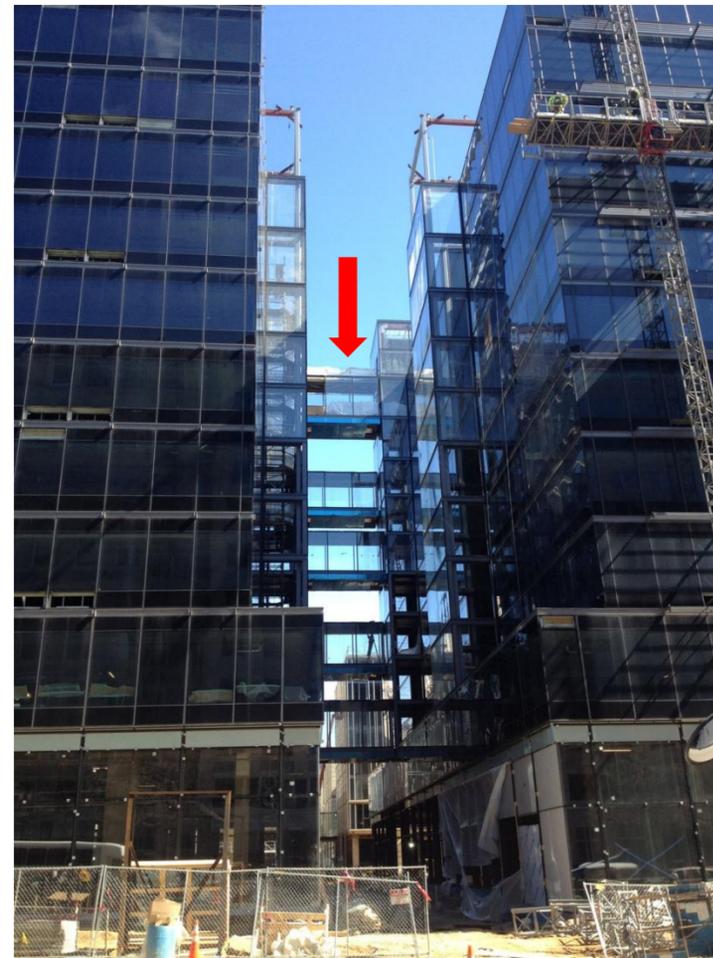
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Alternative Footbridge Installation

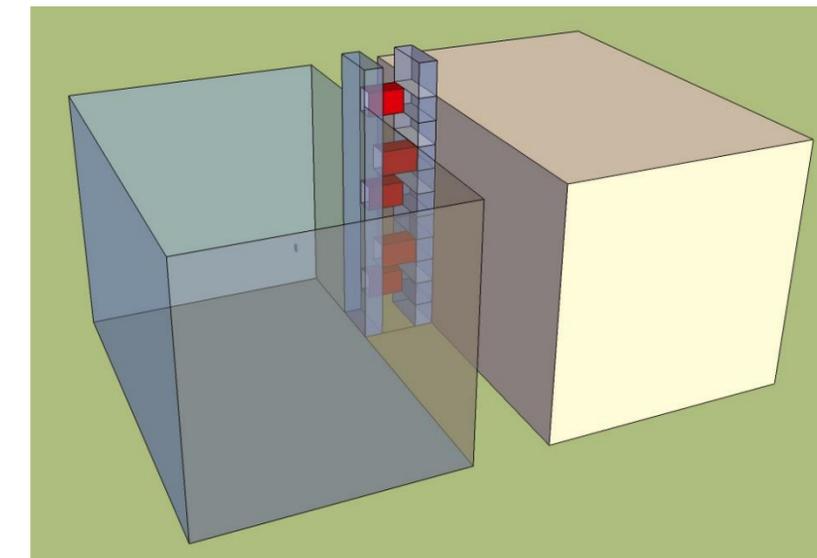
Analysis #3: Footbridges

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- 5 footbridges in between office buildings
 - Steel
 - Curtain wall
- On floors 3,5,7,9, & 11



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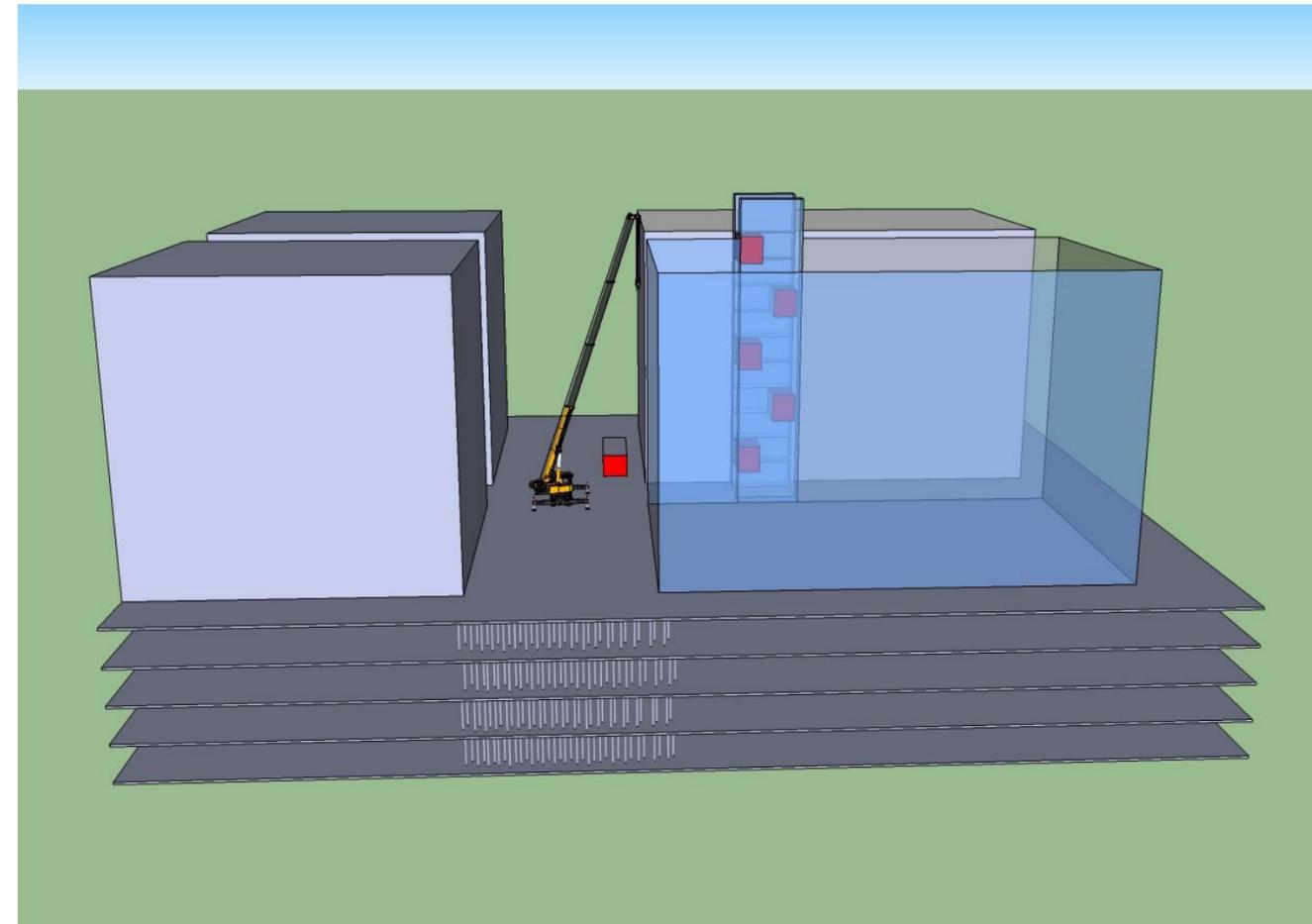
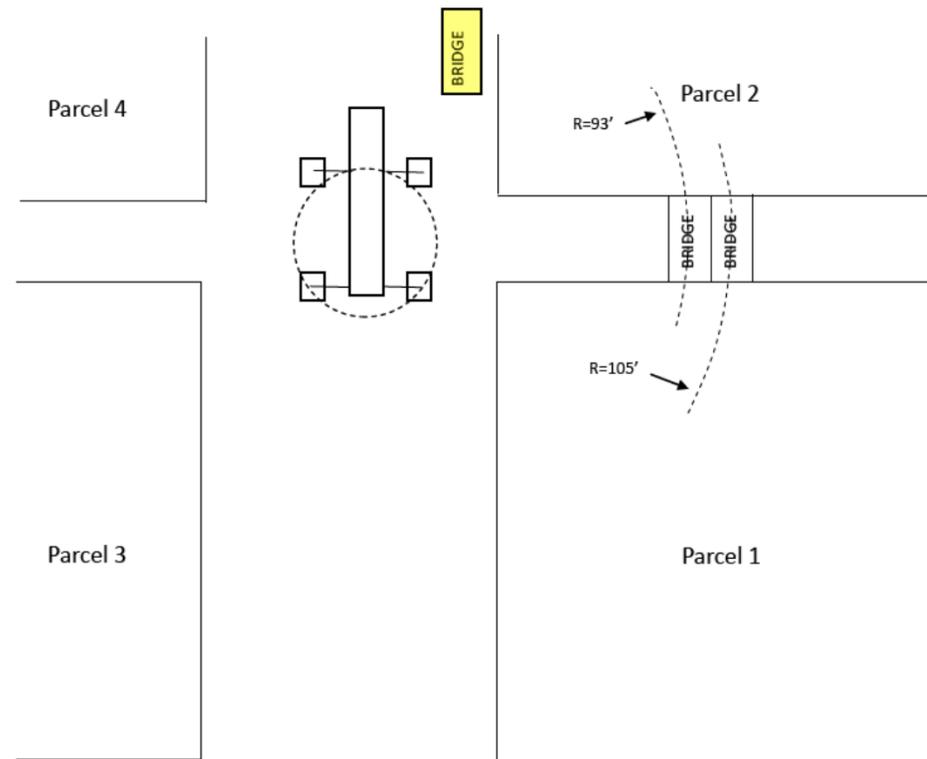


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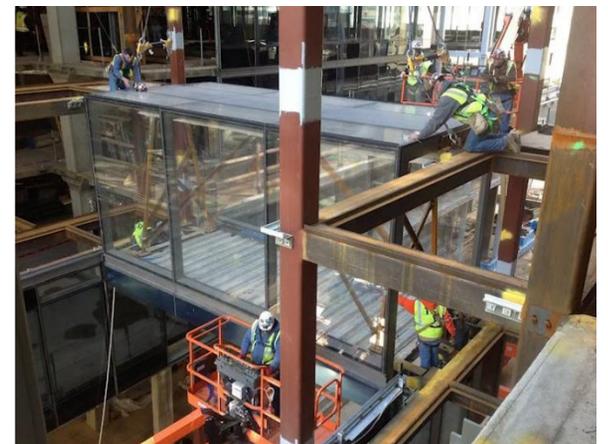
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- ### Bridges
- Prefabrication
 - Including curtain wall
 - Too much risk building in place
 - 20' long/each
 - 36,666 lbs./each

- ### Crane
- 500 ton mobile
 - 220,500 lbs counterweight
 - 138' jib length
 - 51,717 lifting capacity
 - Shoring underneath

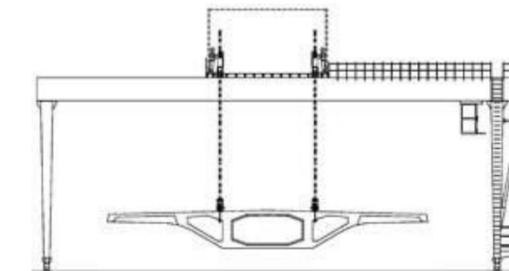




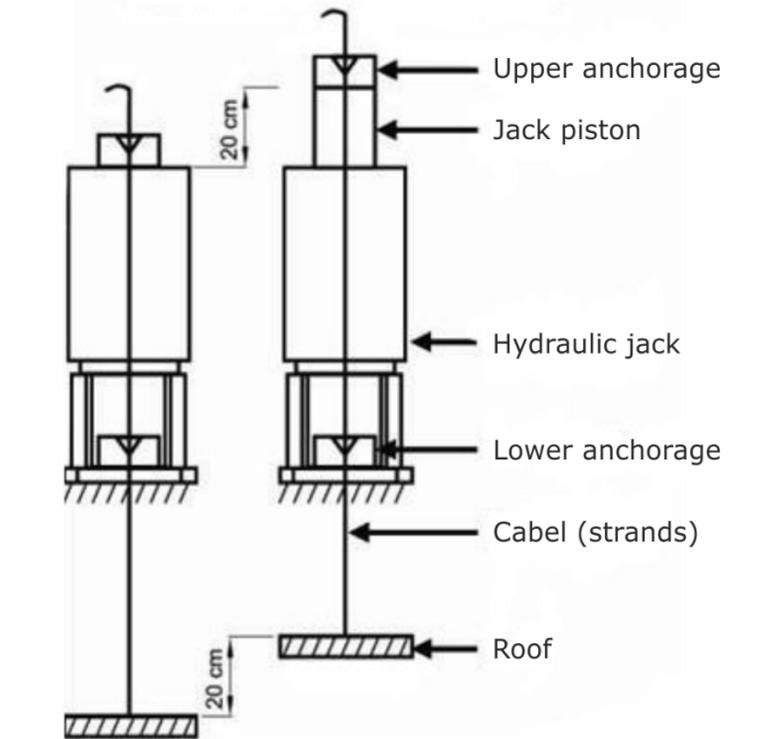
VSL Heavy Lifting

“For projects where notable weight, dimensions, or space limitations exclude the use of cranes or other conventional handling.” (VSL)

- Hydraulic jacks
 - Piston
 - Tensile member
- Gauges and control systems
 - Synchronized movement
- 20 m/hr
- Up to 10,000 tons



VSL strand jack lifting system



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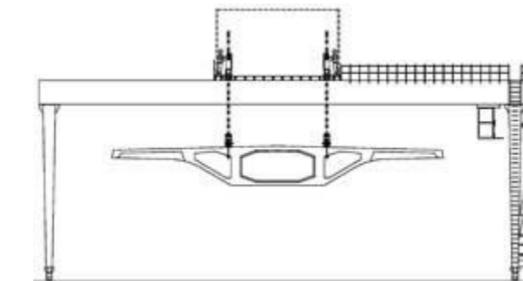
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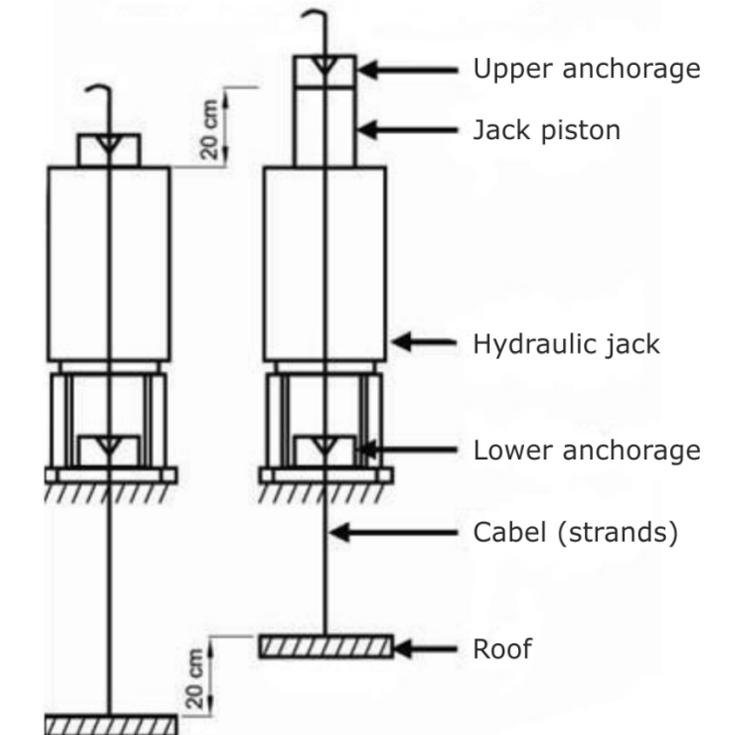
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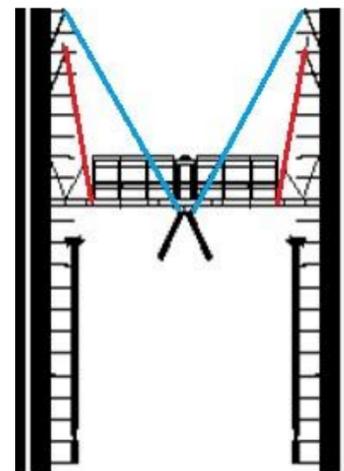
Acknowledgements

Damas Tower Footbridge



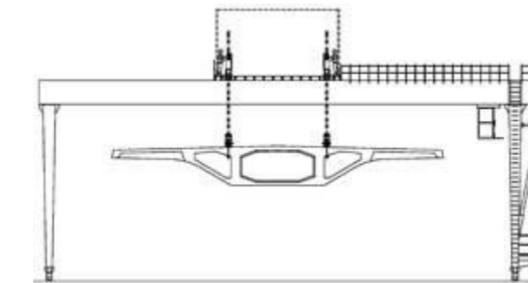
VSL Heavy Lifting

“For projects where notable weight, dimensions, or space limitations exclude the use of cranes or other conventional handling.” (VSL)

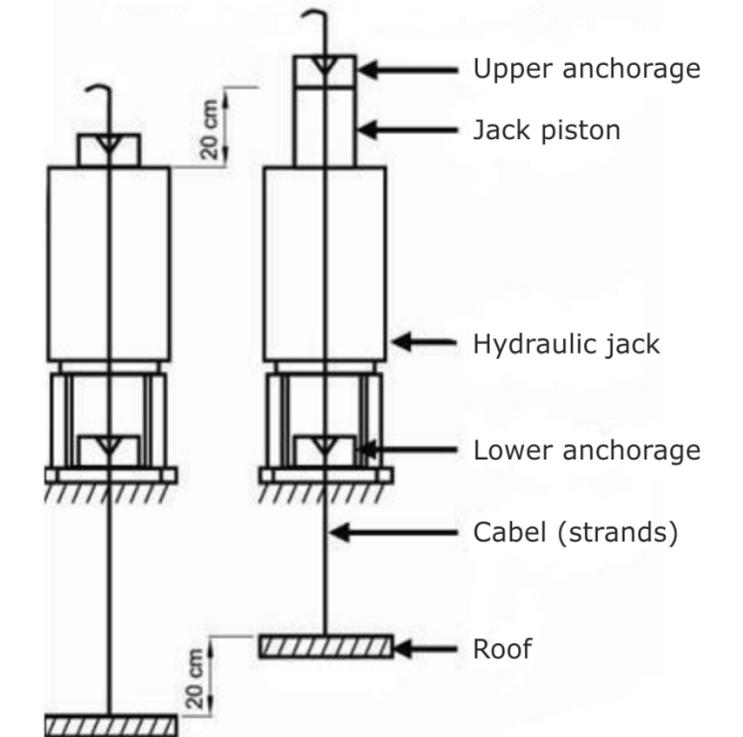


Petronas Towers

- Hydraulic jacks
 - Piston
 - Tensile member
- Gauges and control systems
 - Synchronized movement
- 20 m/hr
- Up to 10,000 tons



VSL strand jack lifting system



Analysis #3: Footbridges

Application

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Washington, D.C.



Project Overview

Analysis #1: SIPS

- Background Information
- New Phasing & SIPS
- Impact

Analysis #2: Electrical Redesign

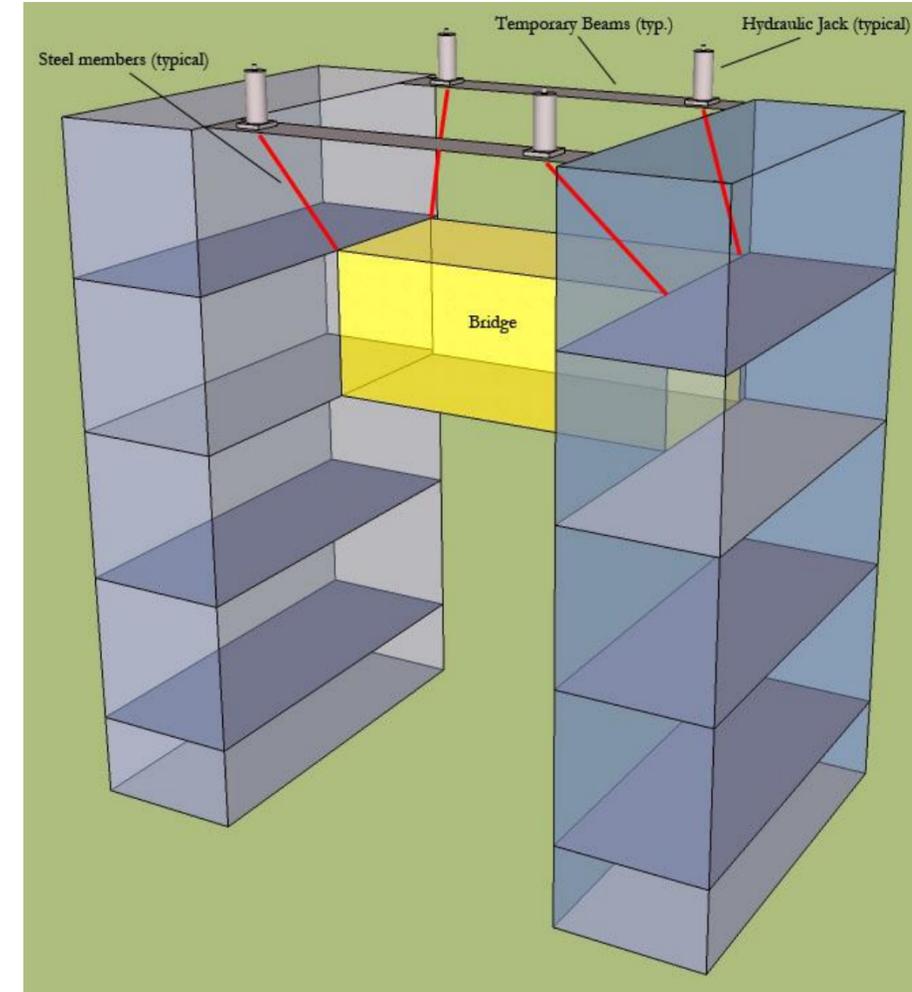
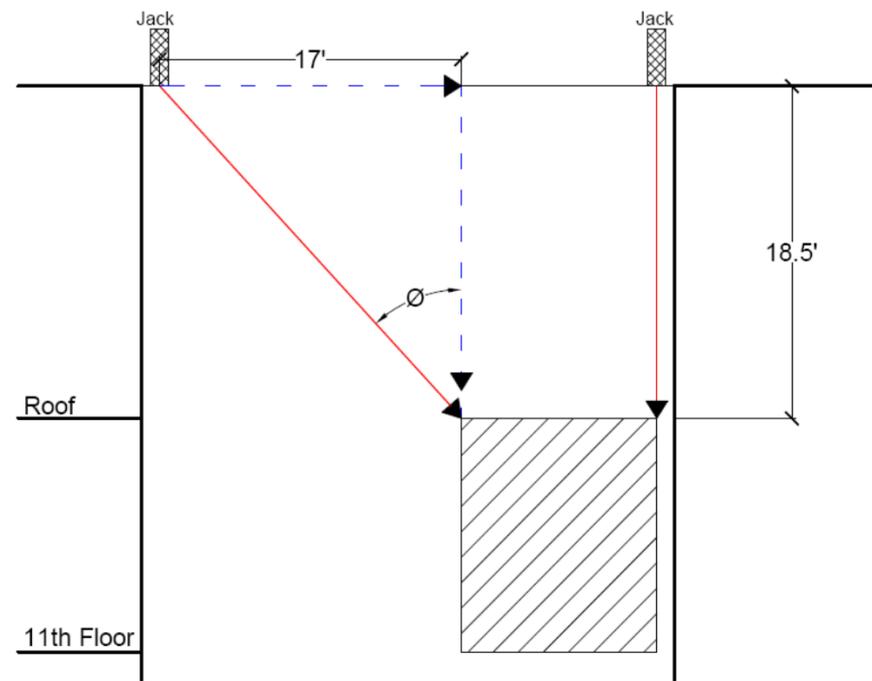
- Background Information
- Redesign
- Impact

Analysis #3: Footbridge Installation

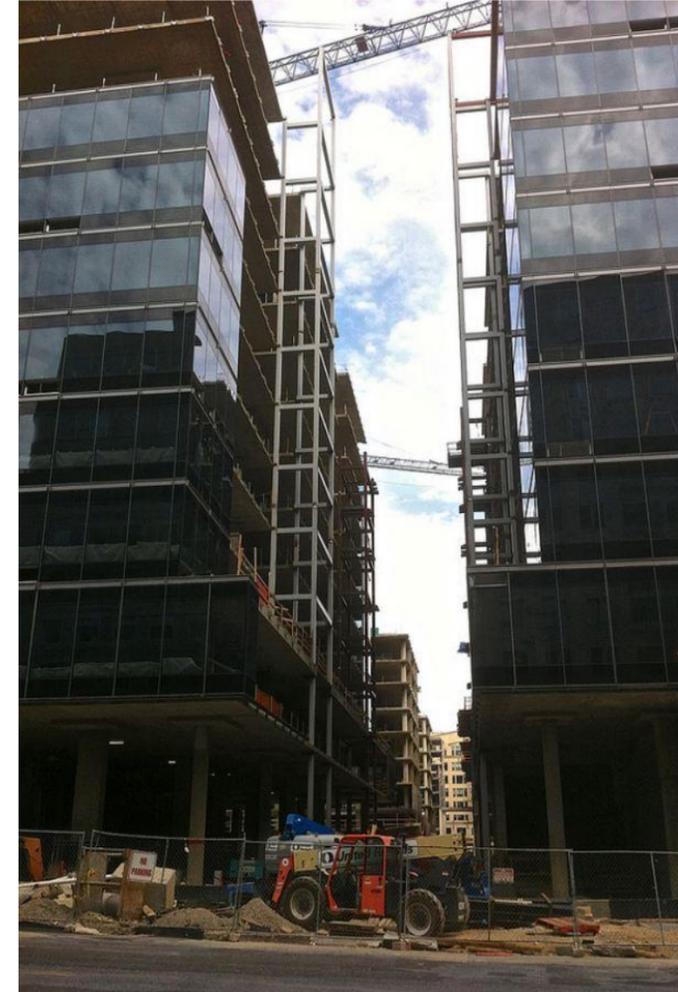
- Background Information
- Research
- Application**
- Results

Final Recommendations

Acknowledgements



- 4 jacks
- Temporary beams span between atriums
- Structural Considerations
 - Steel strands
 - Max. force: 12.6 kips
 - Temporary beams
 - Moment: 25.2 ft k
 - Column buckling
 - F.S. = 3.4



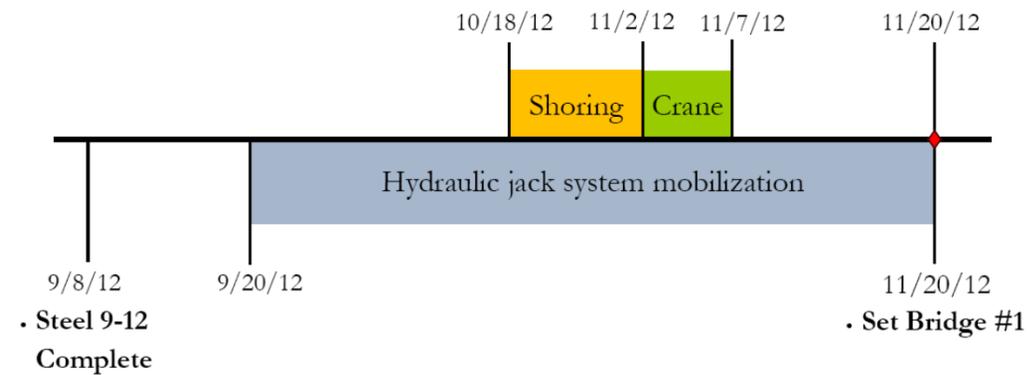


Analysis #3: Footbridges

Results

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Schedule



Project Overview

Analysis #1: SIPS

Background Information

New Phasing & SIPS

Impact

Analysis #2: Electrical Redesign

Background Information

Redesign

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Analysis #3: Footbridge Installation

Background Information

Research

Application

Results

Final Recommendations

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Analysis #3: Footbridges

Results

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Project Overview

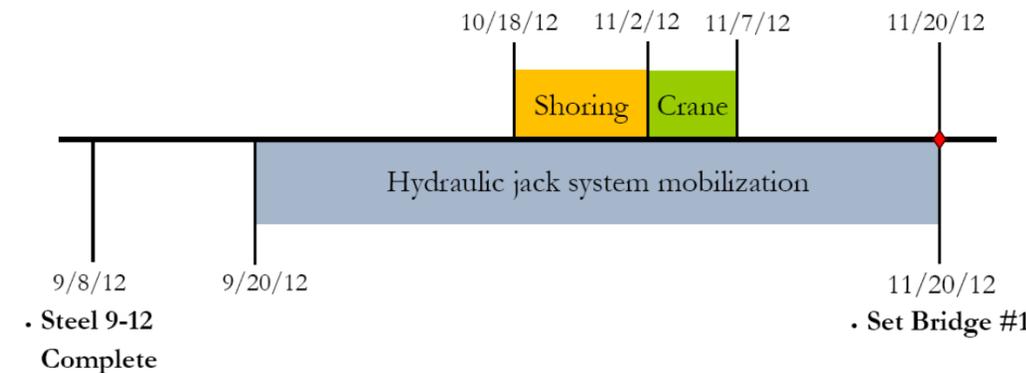
Analysis #1: SIPS
Background Information
New Phasing & SIPS
Impact

Analysis #2: Electrical Redesign
Background Information
Redesign
Impact

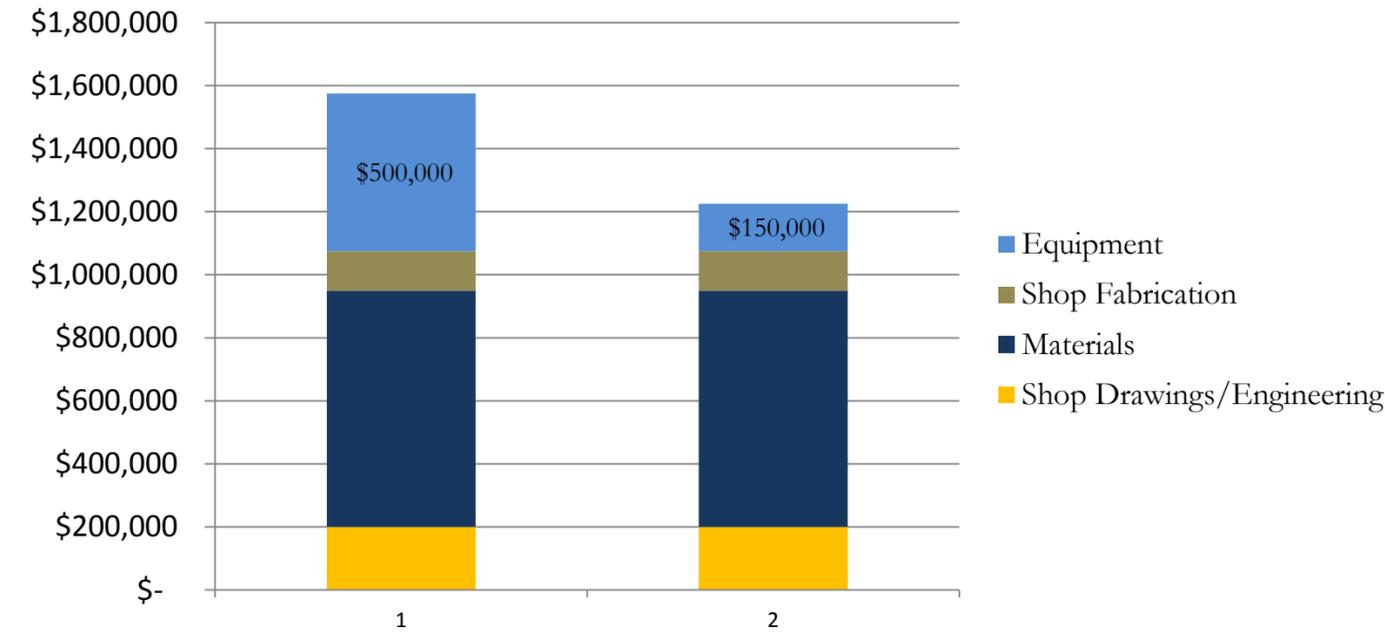
Analysis #3: Footbridge Installation
Background Information
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Application
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Acknowledgements

Schedule



Cost



Constructability

- Guide cables
- Prefabricate bridges onsite
 - 17 days/bridge
 - On portable platform



Conclusion

Project Overview

Analysis #1: SIPS

Background Information

New Phasing & SIPS

Impact

Analysis #2: Electrical Redesign

Background Information

Redesign

Impact

Analysis #3: Footbridge Installation

Background Information

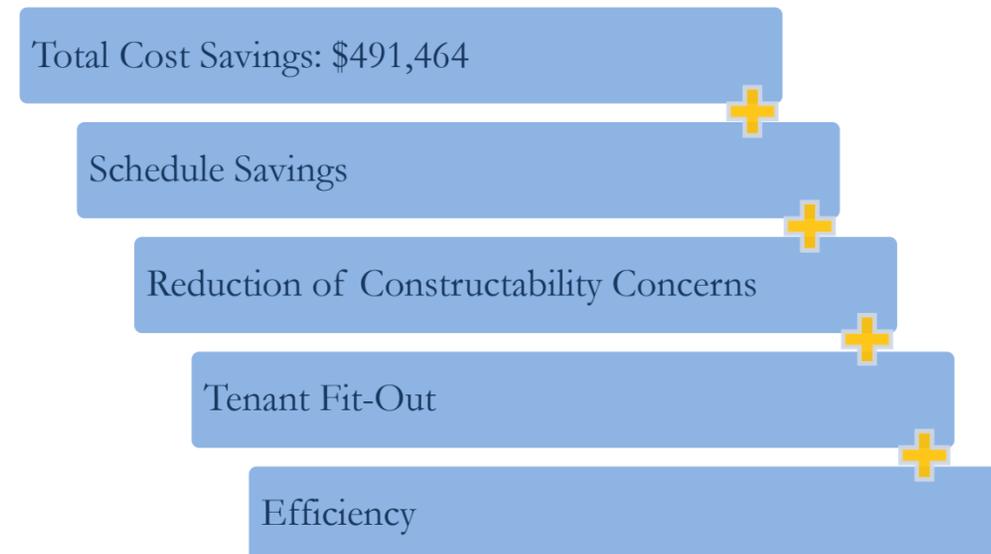
Research

Application

Results

Final Recommendations

Acknowledgements



Analysis #1: SIPS

- Decrease schedule by 13 days
- General conditions savings
- Efficient use of floor space

Analysis #2: Construction Analysis of Electrical Redesign

- Material & labor savings
- Easier system to install
- Reduction of crew size

Analysis #3: Alternative Footbridge Construction

- Major equipment cost savings
- Fewer constructability concerns
 - No schedule impact



Acknowledgements

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Thank You!

Special Thanks

- Family & Friends
- CityCenterDC Project Team
- PACE Industry Members
 - Al Hedin
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- Mike Current

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- Dr. Robert Leicht
- Dr. Richard Mistrick
 - Bob Holland
- Ronald Dodson
 - Kevin Parfitt

Industry

- Clark Construction
 - Truland
 - Hines
 - TSI
 - VSL

Project Overview

Analysis #1: SIPS

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New Phasing & SIPS

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Analysis #2: Electrical Redesign

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Impact

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New Phasing & SIPS

Impact

Analysis #2: Electrical Redesign

Background Information

Redesign

Impact

Analysis #3: Footbridge Installation

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Acknowledgements

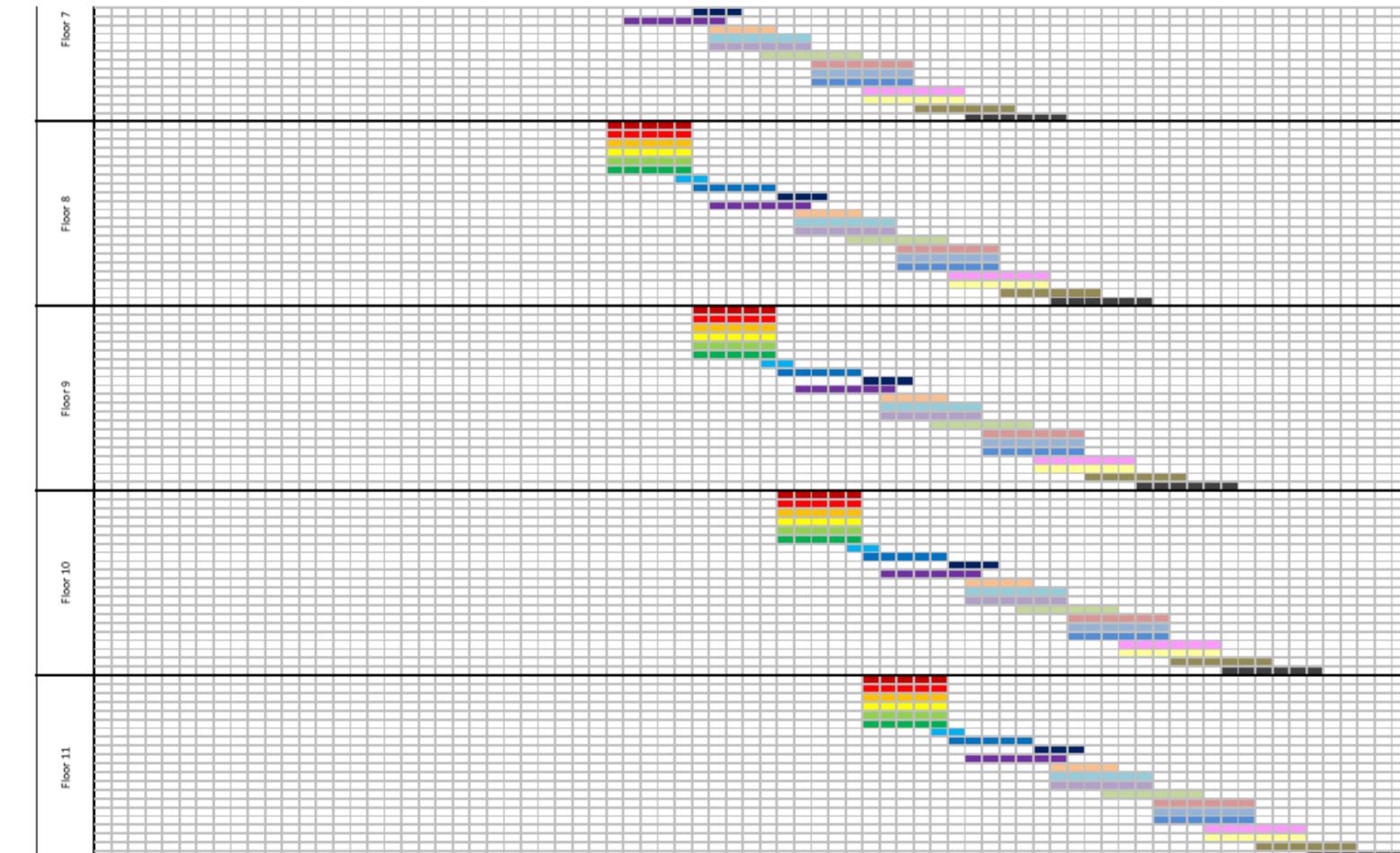
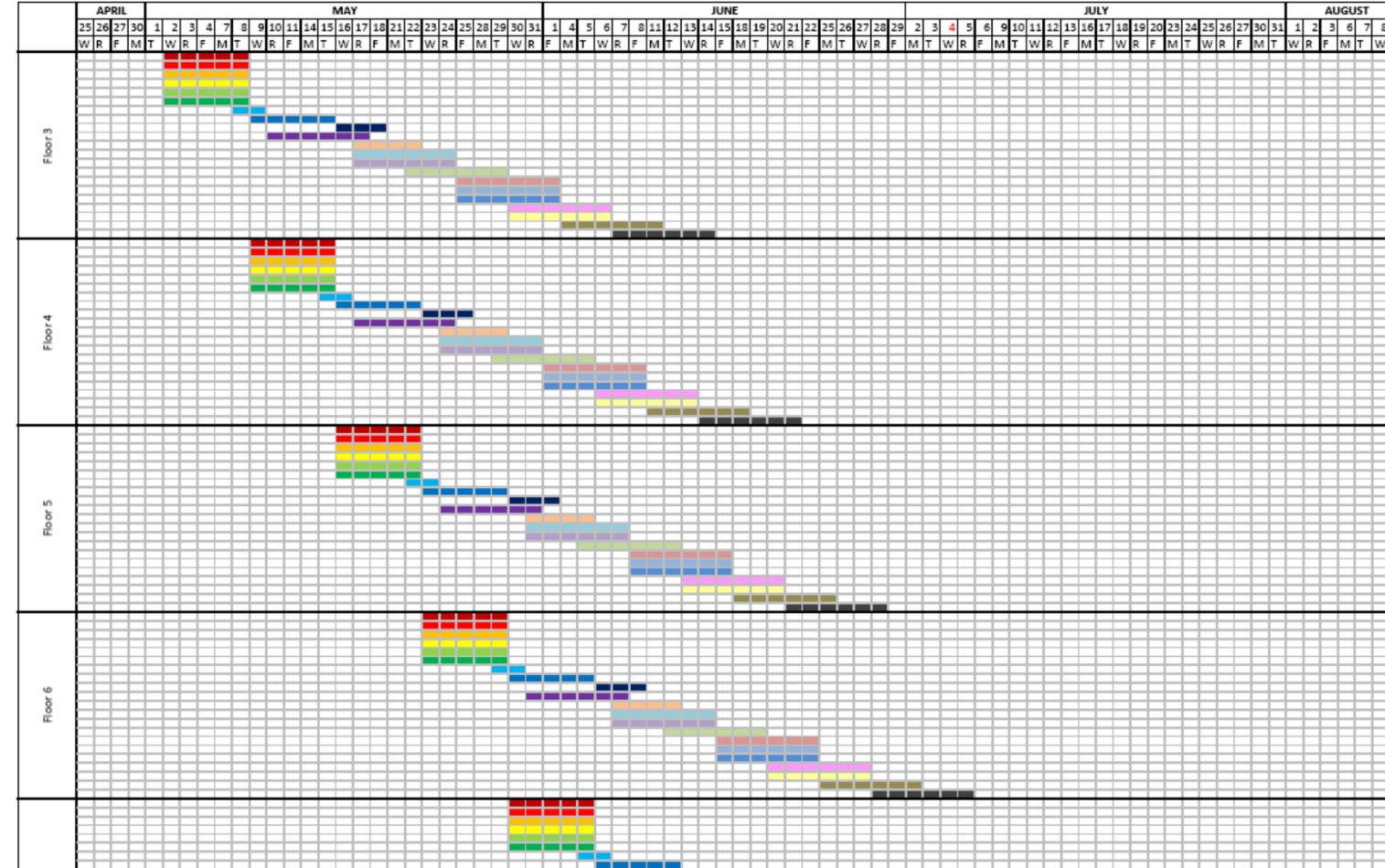




Appendix

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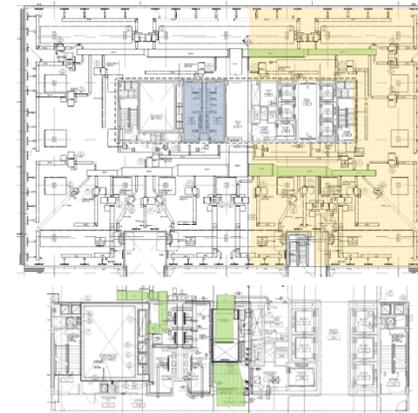
6	Install AHU	2	5/29/2012	5/30/2012	2
6	Frame & Hang Shaft Walls	5	5/31/2012	6/6/2012	5
6	Close In Shafts	3	6/7/2012	6/11/2012	3
6	Layout & Top Track	5	6/1/2012	6/8/2012	6
6	Install Lavatory Support Steel	3	6/8/2012	6/13/2012	4
6	Rough In Duct Mains	5	6/8/2012	6/15/2012	6
6	Install VAV boxes	5	6/8/2012	6/15/2012	6
6	Frame Walls	5	6/15/2012	6/22/2012	6
6	Mechanical Pipe Rough In	5	6/22/2012	6/29/2012	6
6	Plumbing Rough In	5	6/22/2012	6/29/2012	6
6	Duct Rough In	5	6/22/2012	6/29/2012	6
6	Sprinkler Rough In	5	6/29/2012	7/6/2012	5
6	Frame Ceilings	5	7/6/2012	7/13/2012	6
6	Fire Alarm Rough In	5	7/13/2012	7/20/2012	6
6	Electrical Rough In	5	7/13/2012	7/20/2012	6
7	Install Sprinkler Standpipes	5	5/31/2012	6/6/2012	5
7	Duct Riser Rough In	5	5/31/2012	6/6/2012	5
7	Plumbing Riser Rough In	5	5/31/2012	6/6/2012	5
7	Mechanical Riser Rough In	5	5/31/2012	6/6/2012	5
7	Telecom/Security Riser Rough In	5	5/31/2012	6/6/2012	5
7	Electrical Riser Rough In	5	5/30/2012	6/5/2012	5
7	Install AHU	2	6/1/2012	6/5/2012	3
7	Frame & Hang Shaft Walls	5	6/7/2012	6/13/2012	5
7	Close In Shafts	3	6/14/2012	6/18/2012	3
7	Layout & Top Track	5	6/8/2012	6/15/2012	6
7	Install Lavatory Support Steel	3	6/15/2012	6/20/2012	4
7	Rough In Duct Mains	5	6/15/2012	6/22/2012	6
7	Install VAV boxes	5	6/15/2012	6/22/2012	6
7	Frame Walls	5	6/22/2012	6/29/2012	6
7	Mechanical Pipe Rough In	5	6/29/2012	7/6/2012	5
7	Plumbing Rough In	5	6/29/2012	7/9/2012	6
7	Duct Rough In	5	6/29/2012	7/9/2012	6
7	Sprinkler Rough In	5	7/9/2012	7/16/2012	6
7	Frame Ceilings	5	7/16/2012	7/23/2012	6
7	Fire Alarm Rough In	5	7/23/2012	7/30/2012	6
7	Electrical Rough In	5	7/23/2012	7/30/2012	6
8	Install Sprinkler Standpipes	5	7/7/2012	7/13/2012	5
8	Duct Riser Rough In	5	7/7/2012	7/13/2012	5
8	Plumbing Riser Rough In	5	7/7/2012	7/13/2012	5
8	Mechanical Riser Rough In	5	7/7/2012	7/13/2012	5
8	Telecom/Security Riser Rough In	5	7/7/2012	7/13/2012	5
8	Electrical Riser Rough In	5	6/6/2012	6/12/2012	5
8	Install AHU	2	6/14/2012	6/15/2012	2
8	Frame & Hang Shaft Walls	5	6/14/2012	6/20/2012	5
8	Close In Shafts	3	6/21/2012	6/25/2012	3
8	Layout & Top Track	5	6/15/2012	6/22/2012	6
8	Install Lavatory Support Steel	3	6/22/2012	6/27/2012	4



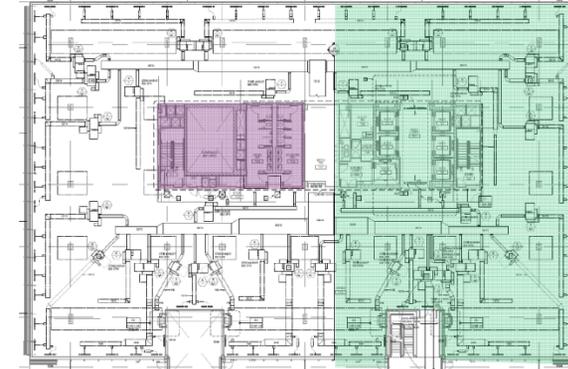


Appendix

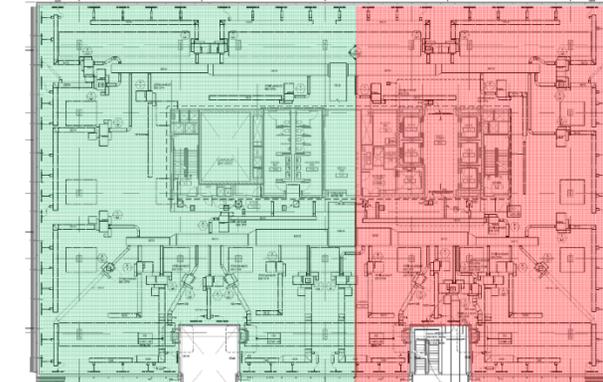
CityCenterDC | Parcel 1
Washington, D.C.



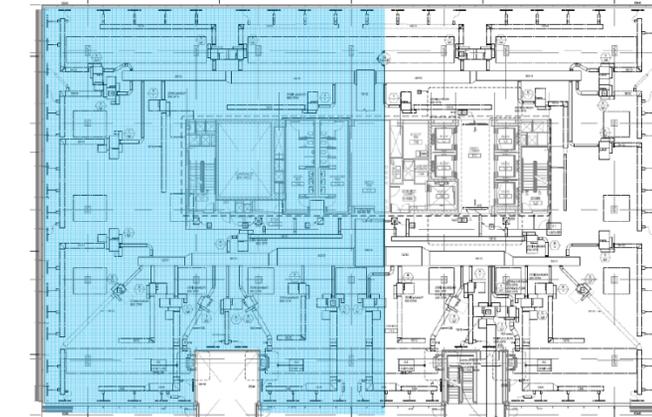
Rough In Duct Mains & Install VAV Boxes AND Lavatory Steel



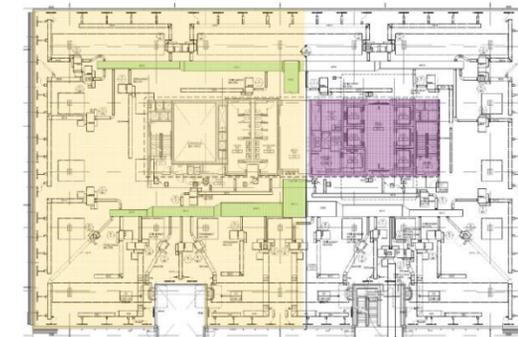
Frame Walls AND Mechanical Pipe, Plumbing, Duct Rough In



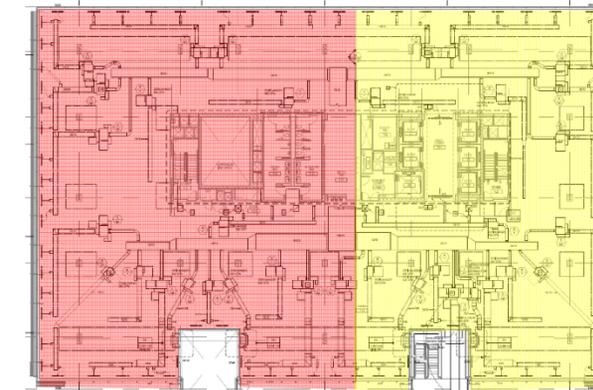
Mechanical Pipe, Plumbing, Duct Rough In AND Electrical and Fire Alarm Rough In



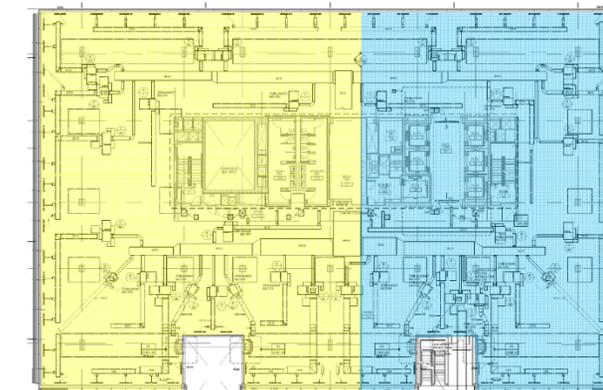
Finish Framing Ceilings



Rough In Duct Mains & Install VAV Boxes AND Frame Walls



Electrical and Fire Alarm Rough In AND Sprinkler Rough In



Sprinkler Rough In AND Frame Ceilings





Appendix

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Table 1. ASHRAE/IES 90.1 lighting power allowances using the Building Area Method.

Building Type	Maximum Lighting Power Density (W/sq.ft.) Allowed Per Version of the ASHRAE/IES 90.1 Standard			
	1989	1999/2001	2004/2007	2010
Automotive Facility	0.96	1.5	0.9	0.982
Convention Center	2.07	1.4	1.2	1.08
Court House	1.44	1.4	1.2	1.05
Dining: Bar	1.37	1.5	1.3	0.99
Lounge/Leisure				
Dining: Cafeteria/Fast Food	1.37	1.8	1.4	0.90
Dining: Family	1.37	1.9	1.6	0.89
Dormitory	1.15	1.5	1.0	0.61
Exercise Center	2.07	1.4	1.0	0.88
Gymnasium	2.07	1.7	1.1	1.00
Healthcare Clinic	1.44	1.6	1.0	0.87
Hospital	1.44	1.6	1.2	1.21
Hotel	1.15	1.7	1.0	1.00
Library	1.29	1.5	1.3	1.18
Manufacturing Facility	0.96	2.2	1.3	1.11
Motel	1.15	2.0	1.0	0.88
Motion Picture Theater	2.07	1.6	1.2	0.83
Multi-Family	1.15	1.0	0.7	0.60
Museum	2.07	1.6	1.1	1.06
Office	1.26	1.3	1.0	0.90
Parking Garage	1.03	0.3	0.3	0.25
Penitentiary	1.44	1.2	1.0	0.97
Performing Arts Theatre	2.07	1.5	1.6	1.39
Police/Fire Station	1.44	1.3	1.0	0.96
Post Office	1.44	1.6	1.1	0.87
Religious Building	2.07	2.2	1.3	1.05
Retail	2.25	1.9	1.5	1.40
School/University	1.29	1.5	1.2	0.99
Sports Arena	2.07	1.5	1.1	0.78
Town Hall	1.44	1.4	1.1	0.92
Transportation	2.07	1.2	1.0	0.77
Warehouse	1.03	1.2	0.8	0.66
Workshop	0.96	1.7	1.4	1.20

of receptacle circuits necessary

$$22436SF \cdot 2.5W / SF = 56090W$$

$$56090W / 180 \frac{VA}{rec} = 312rec$$

$$\frac{312rec}{6 \frac{rec}{ckt}} = 52ckts$$

For the 3RD Floor, panels L3A1 & L3B1 have XX spare 70 ckts OK

For remaining floors, top panels have 67 spare ckts, and bottom panels have 70 spare ckts.... OK

Remaining Typical Floor Layout

Original XFMR anticipated max load of 112.5 kVA from low voltage panels, or 4.8 W/SF.

By reducing receptacle power density to 2.5 W/SF, I propose...

Eliminate XFMRs on floors 4, 6, & 8

The low voltage panels on those floors will be fed by the XFMR on the above floor

So,

Current max kVA for low voltage panels is 112.5kVA, or 4.8 W/SF

Receptacle power density changed to 2.5W/SF

Factor in existing 10kVA load, or .4 W/SF...

$$\frac{112.5kVA}{4.8W / SF} = \frac{X}{2.9W / SF}$$

$$X = 68kVA$$

Therefore, a set of panels require 68 kVA

Meaning both sets together will be a total of 136 kVA

Consequently, you will need a 150 kVA XFMR

*Refer to riser diagram for additional wire and breaker sizing

Type of Occupancy	Lighting ^a	Volt-Amperes per Square Foot		Ten-Year Percent Load Growth
		Min. Power	Air Conditioning Electric Nonelectric	
Automobile	1.0-2.0	0	12-20	20-40
General	2.0-4.0	0.5	5-8	20-40
Stage	2.0-4.0	0.5	5-7	20-40
Art gallery	1.5-2.5	0.5	2.0-3.2	20-40
Bank	1.0-1.6	0.5	5-7	20-30
Cinema	1.0-3.0	0.5	6-10	20-40
Church and synagogue	1.0-3.0	0.5	5-7	20-40
Computer area	1.2-2.1	2.5 ^b	12-20	10-20
Department store	3-5	1.5	5-8	20-30
Apartment	2.0-3.5	1.5	2.5-3.2	10-100
Main floor	2.0-3.5	1.5	2.5-3.2	10-100
Shopping (not hotel) 0-3000 ft ²	3.0	5.0	—	30-100
1000-120,000	0.4	0.15	—	30-100
Above 120,000	1.5-2.5	2.0	—	30-100
College (commercial)	1.0-3.5	1.5	—	10-30
Hospital	1.0-2.0	0.5	5-7	2.0-3.2
Hotel	1.0-1.5	1.0	5-8	2.0-3.5
Lobby	2.0-3.0	5-20	3-5	1.5-2.5
Floors (no cooking)	1.2-2.2	0.5	—	30-60
Residential building	1.5-3.0	1.5	6-10	2.5-4.5
Classrooms	1.0-2.0	0.5	5-7	2.2-2.2
Classroom	1.5-2.5	2.5	4-7	1.5-3.2
Classroom	1.2-2.5	0.5	4-7	1.5-3.2
Classroom	1.5-2.8	2.5	6-10	2.5-4.5
Office building	2.0-2.5	2.0	3.5-5.0	1.5-2.2
Office	2.0-3.5	0.5	—	20-40
Shop	2.0-3.0	0.5	—	20-40
Barber and beauty	2.0-3.0	0.5	3-4	40-80
Dish	2.0-3.5	0.25	—	—
Drug	0.25-1.0	—	4-7	1.5 to 3.2
Fit and spa	0.3	—	—	10-30
Fit, shoe, specialty	0.25	—	—	—
Warehouse (storage)	0.5	—	—	—
In the above except single dwellings:	0.25	—	—	—
Halls, closets, corridors, storage spaces	0.25	—	—	—



Appendix

Switchboard MS12A resize

Capacity:

Lighting & Receptacle Capacity: 1902 kVA

$$1902kVA = \frac{kW}{1000 \cdot 0.95} = 1807000W$$

$$\Rightarrow \frac{1807000W}{257500SF} = 7.02W/SF \text{ Capacity}$$

Recommendations:

ASHRAE, Sec. 9, provides maximum lighting power density recommendation for office building (W/SF)

- ASHRAE 2007 = 1.0 W/SF
- ASHRAE 2010 = 0.9 W/SF

*<http://lightingcontrolsassociation.org/ashrae-releases-90-1-2010-part-1-design-scope-administrative-requirements/>

Per MEEB, pg. 1265, receptacle (misc. power) power density recommendation is: 2.375 W/SF

Therefore,

$$0.9W/SF + 2.375W/SF = 3.275W/SF \text{ for lighting \& receptacle loads}$$

Switchboard MS12A provides an excess of 3.645 W/SF for these loads

Proposal:

Remove 800kVA from lighting & receptacle loads

From 1902kVA to 1102kVA

$$1102kVA \cdot 1000 \cdot 0.95 = 1046900W$$

$$\Rightarrow \frac{1046900W}{257500SF} = 4.1W/SF \text{ NEW lighting \& receptacle capacity}$$

This is still 0.8 W/SF more than design recommendations

Note: A PF of 0.95 was used in all calculations

Effect:

Initial Switchboard total kVA load: 3173 kVA (S982A @ 460V, 3φ)

Revised Switchboard total kVA load: 2373 kVA (2978A @ 460V, 3φ)

Therefore:

You can go from 4000A switchboard to 3000A switchboard!!

3RD Floor Redesign

XFMR

Square footage of office space (minus core) = 22,436 SF

Panels L3A1 & L3B1 (120/208V) are designated for receptacles + already designated loads

So,

$$2.5W/SF \cdot 22436SF = 56090W$$

$$\frac{56090W}{0.95PF} = 59042kVA \approx 59kVA$$

$$\text{Add in existing circuit loads } 59kVA + 10kVA + 0kVA = 69kVA$$

(10kVA from panel L3A1 and 0kVA from panel L3B1)

Therefore, transformer can be reduced from 112.5 kVA to **75 kVA**

Which means your primary breaker can be 100A and your secondary breaker can be or 250A

See PAGES XXX FOR PANEL SCHEDULES

H3MA1

Consolidation of panels H3MA1 & H3MB1

See **Floors 3-9 480V panel consolidation** section

Wiring

Refer to riser diagram

All calculations based off NFPA 70 – NEC 2011



Appendix

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PANEL H(3-11)L1														
BREAKER INTERRUPTING RATING: SERIES RATED														
CONDUIT SIZE	WIRE SIZE	SERVING	KVA A Ø	KVA B Ø	KVA C Ø	CKT BKR	CKT NO	CKT NO	CKT BKR	KVA A Ø	KVA B Ø	KVA C Ø	SERVING	
1 1/2"	2#12	TOILET RM. LTS	1.34			1P-20	1	2	1P-20	1.00			LIT. RELAY PANEL	
1 1/2"	2#12	CORRIDOR LTS	0.36				3	4					SPACE	
		SPACE					5	6						
							7	8						
							9	10						
							11	12						
							13	14						
		V				V	15	16	V				V	
		SPACE					17	18					SPACE	
							19	20						
							21	22						
							23	24						
							25	26						
							27	28						
							29	30						
							31	32						
							33	34						
							35	36						
							37	38	3P-12S	1.82			112.5 KVA XFMR (PANEL LX1A)	
							39	40		0.54				
		V					41	42					0.50	
			1.3	0.4	0.0				2.8	0.5	0.5			
			A Ø = 4 KVA				C Ø = 1 KVA							
			B Ø = 1 KVA				B Ø = 13 KVA				TOTAL = 5 KVA			

PANEL H(3-9)MB1														
BREAKER INTERRUPTING RATING: SERIES RATED														
CONDUIT SIZE	WIRE SIZE	SERVING	KVA A Ø	KVA B Ø	KVA C Ø	CKT BKR	CKT NO	CKT NO	CKT BKR	KVA A Ø	KVA B Ø	KVA C Ø	SERVING	
3/4"	#12	FPTU (C/5.8)	2.51	2.51		3P-15	1	2					SPACE	
							3	4						
							5	6						
							7	8						
							9	10						
							11	12						
							13	14						
							15	16						
							17	18						
							19	20						
							21	22						
							23	24						
							25	26						
							27	28						
							29	30						
							31	32						
							33	34						
							35	36						
							37	38						
							39	40						
		V					41	42					V	
			12.9	12.9	12.9				0.0	0.0	0.0			
			A Ø = 13 KVA				C Ø = 13 KVA				TOTAL = 39 KVA			
			B Ø = 13 KVA				B Ø = 13 KVA				TOTAL = 39 KVA			

NOTE: CONTRACTOR SHALL LABEL ALL FPTU CIRCUITS WITH MECHANICAL ZONE DESIGNATIONS (E.G. "FPTU 2-1"). REFER TO MECHANICAL DRAWINGS FOR ZONE DESIGNATIONS.

PANEL H3MA1														
BREAKER INTERRUPTING RATING: SERIES RATED														
CONDUIT SIZE	WIRE SIZE	SERVING	KVA A Ø	KVA B Ø	KVA C Ø	CKT BKR	CKT NO	CKT NO	CKT BKR	KVA A Ø	KVA B Ø	KVA C Ø	SERVING	
		SPACE					1	2	1P-30	5.82			FPTU (B/5.0)	
							3	4		5.82			FPTU (B/5.0)	
							5	6		5.82			FPTU (B/5.0)	
							7	8		5.82			FPTU (B/5.0)	
							9	10		5.22			FPTU (B/4.4)	
							11	12		5.22			FPTU (B/4.4)	
							13	14	V	5.22			FPTU (B/4.4)	
							15	16	1P-25	4.72			FPTU (B/3.9)	
							17	18		4.72			FPTU (B/3.9)	
							19	20		4.42			FPTU (B/3.9)	
							21	22	V	4.52			FPTU (B/3.7)	
							23	24	1P-30	3.42			FPTU (B/2.9)	
							25	26		3.42			FPTU (B/2.9)	
							27	28		1.64			FPTU (B/-)	
3/4"	2#10	FPTU (B/5.0)					29	30		1.64			FPTU (B/-)	
		FPTU (B/5.0)	5.82				31	32		1.64			FPTU (B/-)	
		FPTU (B/5.0)	5.82				33	34		1.64			FPTU (B/-)	
		FPTU (B/5.0)	5.82				35	36	V	1.64			FPTU (B/-)	
		FPTU (C/4.8)	6.22				37	38	1P-15	3.00			EW-1 (9.0 KW)	
		FPTU (C/4.8)	6.22				39	40		3.00				
		FPTU (C/4.8)	6.22				41	42		3.00				
		V					43	44		3.00				
			12.0	12.0	17.0				29.3	29.6	25.5			
			A Ø = 41 KVA				C Ø = 45 KVA				TOTAL = 123 KVA			
			B Ø = 39 KVA				B Ø = 13 KVA				TOTAL = 123 KVA			

NOTE: CONTRACTOR SHALL LABEL ALL FPTU CIRCUITS WITH MECHANICAL ZONE DESIGNATIONS (E.G. "FPTU 2-1"). REFER TO MECHANICAL DRAWINGS FOR ZONE DESIGNATIONS.

PANEL L(3-11)A1														
BREAKER INTERRUPTING RATING: 10,000 A.I.C.														
CONDUIT SIZE	WIRE SIZE	SERVING	KVA A Ø	KVA B Ø	KVA C Ø	CKT BKR	CKT NO	CKT NO	CKT BKR	KVA A Ø	KVA B Ø	KVA C Ø	SERVING	
1 1/2"	2#12	CORE RECP	1.44			1P-20	1	2	1P-20	0.18			SEC. PNL (5 & 10)	
							3	4		1.80			W. SLOT TRK (5)	
							5	6					1.00 W. SLOT LED (5 & 6)	
							7	8		1.00			E. SLOT (3-6, 11)	
							9	10		1.46			E. SLOT LED (10, 11)	
							11	12					SPACE	
							13	14						
							15	16						
							17	18						
							19	20						
							21	22						
							23	24						
							25	26						
							27	28						
							29	30	V				V	
							31	32					SPACE	
							33	34						
							35	36						
							37	38						
							39	40						
							41	42						
		V					43	44					V	
			1.9	1.0	1.0				1.2	3.3	1.1			
			A Ø = 3 KVA				C Ø = 2 KVA				TOTAL = 10 KVA			
			B Ø = 4 KVA				B Ø = 13 KVA				TOTAL = 10 KVA			

NOTE: CONTRACTOR SHALL LABEL ALL FPTU CIRCUITS WITH MECHANICAL ZONE DESIGNATIONS (E.G. "FPTU 2-1"). REFER TO MECHANICAL DRAWINGS FOR ZONE DESIGNATIONS.

PANEL L(2-11)B1														
BREAKER INTERRUPTING RATING: 10,000 A.I.C.														
CONDUIT SIZE	WIRE SIZE	SERVING	KVA A Ø	KVA B Ø	KVA C Ø	CKT BKR	CKT NO	CKT NO	CKT BKR	KVA A Ø	KVA B Ø	KVA C Ø	SERVING	
		SPACE				1P-20	1	2	1P-20				SPACE	
							3	4						
							5	6						
							7	8						
							9	10						
							11	12						
							13	14						
							15	16						
							17	18						
							19	20						
							21	22						
							23	24						
							25	26						
							27	28						
							29	30	V				V	
							31	32					SPACE	
							33	34						
							35	36						
							37	38						
							39	40						
							41	42						
		V					43	44					V	
			0.0	0.0	0.0				0.0	0.0	0.0			
			A Ø = 0 KVA				C Ø = 0 KVA				TOTAL = 0 KVA			
			B Ø = 0 KVA				B Ø = 13 KVA							



Appendix

CityCenterDC | Parcel 1
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TYPE ¹	CAPACITY²	KEY DATA FOR VSL LIFTING UNITS			
		MAX. NUMBER OF STRANDS	CABLE DIAMETER	OVERALL DIMENSIONS	WEIGHT³
	kN		D(mm)	HxW(mm)	kg
SLU-10	104	1	16	970 200	60
SLU-30	312	3	54	1130 250	120
SLU-40	416	4	67	1275 250	200
SLU-70	728	7	82	1122 400	230
SLU-120	1248	12	116	1400 400	430
SLU-220	2288	22	167	2100 520	1520
SLU-330	3224	31	190	2140 600	1820
SLU-440	4368	42	228	2050 610	2220
SLU-580	5720	55	254	1780 790	3250

Package 1 - Original									
Description	Length	Count	Mat. \$	Equip. \$	Total Mat. \$	Lbr. Hr.	Lbr. \$	Total Lbr. \$	Total \$
4000A MS12A DISTRIBUTION SWITCHBOARD		1		\$ 67,200.00	\$ 67,200.00	80.5	\$ 45.00	\$ 3,622.50	\$ 70,822.50
225A HXMA1 PANELBOARD		7		\$ 7,600.00	\$ 7,600.00	119	\$ 45.00	\$ 5,355.00	\$ 12,955.00
225A HXMB1 PANELBOARD		7		\$ 4,900.00	\$ 4,900.00	70	\$ 45.00	\$ 3,150.00	\$ 8,050.00
225A HXL1 PANELBOARD		7		\$ 5,400.00	\$ 5,400.00	206.5	\$ 45.00	\$ 9,292.50	\$ 14,692.50
400A LX1 PANELBOARD		7		\$ 10,250.00	\$ 10,250.00	227.5	\$ 45.00	\$ 10,237.50	\$ 20,487.50
400A LXB1 PANELBOARD		7		\$ 5,400.00	\$ 5,400.00	175	\$ 45.00	\$ 7,875.00	\$ 13,275.00
112.5 KVA 3PH 480V STEEL FLEX WITH GROUND		7	\$ 5,364.33		\$ 40,814.33	292.88	\$ 45.00	\$ 13,179.60	\$ 53,993.93
225A CU BUS DUCT		1		\$ 18,450.00	\$ 18,450.00	84.2	\$ 45.00	\$ 3,789.00	\$ 22,239.00
BUS PLUG -> PNL HXMA1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	35*7	1		\$ 6,566.98	\$ 6,566.98	19.94	\$ 45.00	\$ 897.30	\$ 7,464.28
BUS PLUG -> PNL HXL1 - 2 1/2" EMT [40] 3/0, [1] 6GRD CONC T-ROD	28*7	1		\$ 5,017.60	\$ 5,017.60	16.08	\$ 45.00	\$ 723.60	\$ 5,741.20
4000A CU LZ DUCT		390		\$ 245,700.00	\$ 245,700.00	719.9	\$ 45.00	\$ 32,395.50	\$ 278,095.50
Total				\$ 417,298.91	\$ 417,298.91	2,011.50	\$ 90,517.50	\$ 507,816.41	

Package 2 - New									
Description	Length	Count	Mat. \$	Equip. \$	Total Mat. \$	Lbr. Hr.	Lbr. \$	Total Lbr. \$	Total \$
3000A MS12A DISTRIBUTION SWITCHBOARD		1		\$ 40,700.00	\$ 40,700.00	80.5	\$ 45.00	\$ 3,622.50	\$ 44,322.50
225A HXMA1 PANELBOARD		7		\$ 10,500.00	\$ 10,500.00	175	\$ 45.00	\$ 7,875.00	\$ 18,375.00
225A H3L1 PANELBOARD		1		\$ 1,500.00	\$ 1,500.00	28	\$ 45.00	\$ 1,260.00	\$ 2,760.00
225A H4L1 PANELBOARD		3		\$ 4,510.00	\$ 4,510.00	75	\$ 45.00	\$ 3,375.00	\$ 7,885.00
225A H5L1 PANELBOARD		3		\$ 5,800.00	\$ 5,800.00	88.5	\$ 45.00	\$ 3,982.50	\$ 9,782.50
400A L3A1 PANELBOARD		1		\$ 1,170.00	\$ 1,170.00	25	\$ 45.00	\$ 1,125.00	\$ 2,295.00
400A L3B1 PANELBOARD		7		\$ 4,900.00	\$ 4,900.00	175	\$ 45.00	\$ 7,875.00	\$ 12,775.00
600A LX1 PANELBOARD		3		\$ 6,500.00	\$ 6,500.00	102	\$ 45.00	\$ 4,590.00	\$ 11,090.00
600A LXB1 PANELBOARD		3		\$ 3,190.00	\$ 3,190.00	88.5	\$ 45.00	\$ 3,982.50	\$ 7,172.50
75 KVA 3PH 480V STEEL FLEX WITH GROUND		1	\$ 558.27	\$ 4,200.00	\$ 4,758.27	28.81	\$ 45.00	\$ 1,296.45	\$ 6,054.72
150 KVA 3PH 480V STEEL FLEX WITH GROUND		3	\$ 3,612.46	\$ 19,800.00	\$ 23,412.46	145.2	\$ 45.00	\$ 6,534.00	\$ 29,946.46
250A CU BUS DUCT		1		\$ 7,180.00	\$ 7,180.00	18.2	\$ 45.00	\$ 819.00	\$ 7,999.00
200A CU BUS DUCT		1		\$ 16,000.00	\$ 16,000.00	48.2	\$ 45.00	\$ 2,169.00	\$ 18,169.00
100A CU BUS DUCT		1		\$ 4,800.00	\$ 4,800.00	12.2	\$ 45.00	\$ 549.00	\$ 5,349.00
BUS PLUG -> PNL H3MA1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	35	1	\$ 865.17		\$ 865.17	19.42	\$ 45.00	\$ 873.90	\$ 1,739.07
BUS PLUG -> PNL H3L1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	28	1	\$ 716.80		\$ 716.80	16.08	\$ 45.00	\$ 723.60	\$ 1,440.40
BUS PLUG -> PNL H4MA1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	35	1	\$ 840.92		\$ 840.92	18.02	\$ 45.00	\$ 810.90	\$ 1,651.82
BUS PLUG -> PNL H4L1 - 1 1/4" EMT [4] 3, [1] 8GRD CONC T-ROD	28	1	\$ 243.02		\$ 243.02	10.93	\$ 45.00	\$ 491.85	\$ 734.87
BUS PLUG -> PNL H5MA1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	35	1	\$ 840.92		\$ 840.92	18.02	\$ 45.00	\$ 810.90	\$ 1,651.82
BUS PLUG -> PNL H5L1 - 2 1/2" EMT [4] 250, [1] 4 CONC T-ROD	28	1	\$ 1,019.43		\$ 1,019.43	19.27	\$ 45.00	\$ 867.15	\$ 1,886.58
PNL LXB1 -> PNL LX1 - 2 1/2" EMT [4] 3/0, [1] 6GRD CONC T-ROD	10*3	1	\$ 1,291.08		\$ 1,291.08	11.88	\$ 45.00	\$ 534.60	\$ 1,825.68
3000A CU LZ DUCT		390		\$ 163,800.00	\$ 163,800.00	626	\$ 45.00	\$ 28,170.00	\$ 191,970.00
Total				\$ 304,538.07	\$ 304,538.07	1,829.73	\$ 82,337.85	\$ 386,875.92	

Savings \$ 120,940.49

H(3-9)MA1															
V:	480Y/277	Rm #	Elec. Rm	10000	AIC	3P - 4W	Fdr:	(4) 3/0 & #6 G.	2-1/2"C	155 kVA				MLO	
Designations		VA/Phase			Bkr/Pole/Wire			Designations		VA/Phase			Bkr/Pole/Wire		
Ckt	Description	A	B	C	Bkr	# P	W	Ckt	Description	A	B	C	Bkr	# P	W
1	FPTU (C/5.9)	2510			20	3	#12	2	FPTU (B/5.0)	5820			30	1	#10
3	-		2510		-	-	-	4	FPTU (B/5.0)		5820		30	1	#10
5	-			2510	-	-	-	6	FPTU (B/5.0)			5820	30	1	#10
7	FPTU (C/5.9)	2510			20	3	#12	8	FPTU (B/5.0)	5820			30	1	#10
9	-		2510		-	-	-	10	FPTU (B/4.4)		5220		30	1	#12
11	-			2510	-	-	-	12	FPTU (B/4.4)			5220	30	1	#12
13	FPTU (C/6.6)	2740			20	3	#12	14	FPTU (B/4.4)	5220			30	1	#12
15	-		2740		-	-	-	16	FPTU (B/3.9)		4720		25	1	#12
17	-			2740	-	-	-	18	FPTU (B/3.8)			4720	25	1	#12
19	FPTU (C/6.6)	2740			20	3	#12	20	FPTU (B/3.6)	4420			25	1	#12
21	-		2740		-	-	-	22	FPTU (B/3.7)		4520		25	1	#12
23	-			2740	-	-	-	24	FPTU (B/2.6)			3420	20	1	#12
25	Space	0			0	0	#####	26	FPTU (B/2.6)	3420			20	1	#12
27	Space		0		0	0	#####	28	FPTU (B/-)		1640		20	1	#12
29	FPTU (B/5.0)			5820	30	1	#10	30	FPTU (B/-)			1640	20	1	#12
31	FPTU (B/5.0)	5820			30	1	#10	32	FPTU (B/-)	1640			20	1	#12
33	FPTU (B/5.0)		5820		30	1	#10	34	FPTU (B/-)		1640		20	1	#12
35	FPTU (B/5.0)			5820	30	1	#10	36	FPTU (B/-)			1640	20	1	#12
37	FPTU (B/4.6)	6220			30	1	#10	38	EWB-1	3000			20	3	#12
39	FPTU (B/4.6)		6220		30	1	#10	40	-		3000		-	-	-
41	FPTU (B/4.6)			6220	30	1	#10	42	-			3000	-	-	-



Appendix

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+ This cable will take the largest force due to its position & angle. Any bridges @ lower elevation will have smaller force on cable bc angle θ will be smaller.

$\tan \theta = \frac{H}{17}$
 $\theta = 42.6^\circ$
 $\cos 42.6^\circ = \frac{17}{H}$
 $H = 12.6 \text{ k}$
 $\sigma = \frac{F}{A}$
 $\sigma = \frac{12.6}{10.4} = 1212 \text{ psi}$

For SLU-30 (3 strands)
 $A = \pi r^2$
 $D_{strand} = 54 \text{ mm} = 2.1"$
 $R_{strand} = 1.05"$
 $A_{strand} = 3.14 \cdot (1.05)^2 = 3.46 \text{ in}^2 \times 3 \text{ strands} = 10.4 \text{ in}^2$
 $\sigma = \frac{70140}{10.4} = 6744 \text{ psi}$

For SLU-10 (1 strand) choose SLU-10
 $D_{strand} = 16 \text{ mm} = 0.63"$
 $R = .32"$
 $A = 3.14 \cdot (0.32)^2 = 0.32 \text{ in}^2$
 $\sigma = \frac{1160}{0.32} = 3625 \text{ psi}$

Making sure columns don't buckle from added jack load

Tributary Area

Floor + Roof

$A_T = \left(\frac{22}{2}\right)\left(\frac{14}{2}\right) = 77 \text{ ft}^2$

Exterior Wall

$A_T = (11 \times 10) + (11 \times 6) = 176 \text{ ft}^2/\text{Floor}$
 Height = 455 on each side

LL Bed

$0.25 + \frac{15}{216} = .85$
 $.67$
 $.6$
 $.55$
 $.52$
 $.50$
 $.49$
 $.46$
 $.45$

Roof Loads

DL = 10 + 5 + 8 + 9 = 27 psf
 rafter joist 2x12 min/2x12

S = 30 psf

Floor Loads

DL = 60 + 10 + 5 = 75 psf
 wall 2x12 min

LL = 80 psf

Load from curtain wall = 15 psf

HSS 10x10x use conservative KL = 15'

$1.2(27)(77) + 1.6(50)(177) = 6.2 \text{ k}$
 $1.2(27)(77) + 0.5(30)(77) + 1.2(75)(77) + 1.2(15)(176) + 1.6(0.45)(80)(77)/1000 = 22.1 \text{ k}$
 $3.6 + 2(10.1) + 1.6(0.67)(80)(77)(2)/1000 = 37^2 + 9.2^2 = 46.2 \text{ k}$
 $3.6 + 3(10.1) + 1.6(0.6)(80)(77)(3)/1000 = 51.6^2 + 9.2^2 = 60.8 \text{ k}$
 $3.6 + 4(10.1) + 1.6(0.55)(80)(77)(4)/1000 = 65.9^2 + 2(9.2) = 84.1 \text{ k}$
 $3.6 + 5(10.1) + 1.6(0.52)(80)(77)(5)/1000 = 79.7^2 + 2(9.2) = 99.1 \text{ k}$
 $3.6 + 6(10.1) + 1.6(0.5)(80)(77)(6)/1000 = 93.8^2 + 3(9.2) = 121.4$
 $3.6 + 7(10.1) + 1.6(0.48)(80)(77)(7)/1000 = 107.4^2 + 3(9.2) = 155 \text{ k}$
 $3.6 + 8(10.1) + 1.6(0.46)(80)(77)(8)/1000 = 120.7^2 + 4(9.2) = 157.5 \text{ k}$
 $3.6 + 9(10.1) + 1.6(0.45)(80)(77)(9)/1000 = 134.4^2 + 4(9.2) = 171.2 \text{ k}$

* End of steel columns

HSS 10x10x1/2 Capacity = 615 k

ⓐ through ⓓ indicate load from footbridge. One column takes 1/4 of the footbridge weight, or 9.2k

+ place beam to span the two atriums.
 + Hydraulic jacks will then be placed on top of beams
 + use wide flange beam w/ web stiffeners to support jacks

$M = 12.6 \text{ k} \times 2 = 25.2 \text{ k-ft}$

* Use minimum W12x14. Size up if necessary to fit hydraulic jack on.

* Used AISC Steel Construction Manual, 14th edition